This document gives pertinent information concerning the reissuance of the VPDES Permit listed below. This permit is being processed as a Minor, Municipal permit. The discharge results from the operation of a 0.01 MGD wastewater treatment plant. This permit action consists of updating the proposed effluent limits to reflect the current Virginia WQS (effective January 6, 2011) and updating permit language as appropriate. The VPDES Permit also has an additional design flow tier of 0.02 MGD. The effluent limitations and special conditions contained in this permit will maintain the Water Quality Standards of 9VAC25-260 et seq.

1. Facility Name and Mailing

Address:

Fauquier Springs Country Club Wastewater Treatment Plant

P. O. Box 419

Warrenton, VA 20186

Facility Location:

9236 Tournament Drive Warrenton, VA 20186

County:

SIC Code:

Fauquier

4952 WWTP

Facility Contact Name:

Donald Hearl

Telephone Number:

540-825-6660

Facility E-mail Address:

donh@ess-services.com

2. Permit No.:

VA0077411

Expiration Date of previous permit:

December 21, 2013

Other VPDES Permits associated with this facility:

Other Permits associated with this facility:

None None

E2/E3/E4 Status:

NA

3. Owner Name:

Sulphur Springs Investment Corporation

Owner Contact/Title:

Robert Foley/President

Telephone Number:

540-347-2500

Owner E-mail Address:

ljfoley1@comcast.net

4. Application Complete Date:

Permit Drafted By:

July 26, 2013

Joan C. Crowther

Date Drafted:

1/14/14

Draft Permit Reviewed By:

Alison Thompson

Date Reviewed:

1/30/14

Public Comment Period:

Start Date:

2/12/14

End Date:

3/14/14

5. Receiving Waters Information: See Attachment 1 for the Flow Frequency Determination

Receiving Stream Name:

Rappahannock River

Stream Code:

3-RPP

Drainage Area at Outfall:

205.7 sq.mi.

River Mile:

158.41

558

Stream Basin:

Rappahannock River

Subbasin:

None

Section:

3

Stream Class: Waterbody ID:

VAN-E02R

Special Standards:

None

7010 IEak Elaw

VAIN-LOZI

7010 Flow:

1.68 MGD

7Q10 High Flow:

21.3 MGD

1Q10 Flow:

1.42 MGD

1Q10 High Flow:

16.8 MGD

30Q10 Flow:

3.6 MGD

30Q10 High Flow:

30.4 MGD

Harmonic Mean Flow:

25.2 MGD

30Q5 Flow:

6.2 MGD

6. Statutory or Regulatory Basis for Special Conditions and Effluent Limitations:

X	State Water Control Law		EPA Guidelines
X	Clean Water Act	X	Water Quality Standards
X	VPDES Permit Regulation	<u></u>	Other
X	EPA NPDES Regulation		

- 7. Licensed Operator Requirements: Class IV
- Reliability Class: Class II
- 9. Permit Characterization:

X	Private	Effluent Limited	Possible Interstate Effect
	Federal	X Water Quality Limited	Compliance Schedule Required
	State	Whole Effluent Toxicity Program Required _	Interim Limits in Permit
	POTW	Pretreatment Program Required	Interim Limits in Other Document
X	TMDL	e-DMR Participant	

10. Wastewater Sources and Treatment Description:

The wastewater treatment plant consists of septic tank followed by coarse screening, flow equalization, biological treatment (extended aeration), clarification, UV disinfection, and cascade aeration. See flow diagram below.

The Certificate to Operate (CTO) the 0.01 MGD design flow facility was issued on October 6, 2011. The CTO can be found as Attachment 2.

Flow Diagram of Fauquier Springs Country Club WWTP

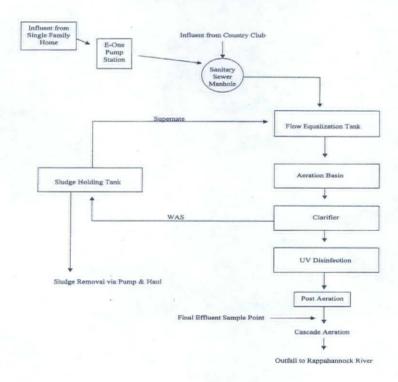
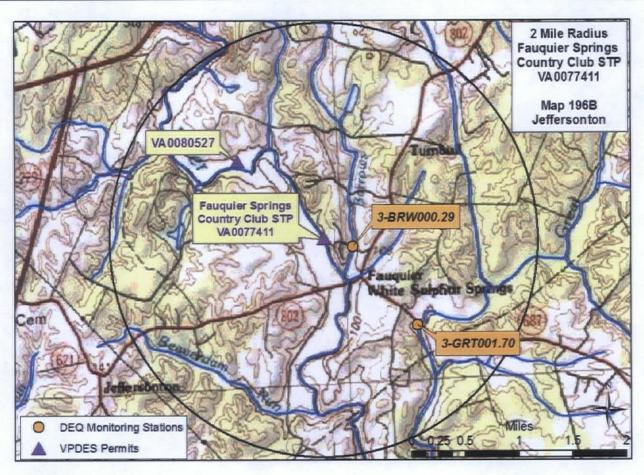


TABLE 1 – Outfall Description							
Outfall Number	Discharge Sources	Treatment	Design Flow(s)	Outfall Latitude and Longitude			
001	Domestic and/or Commercial Wastewater	See Item 10 above.	0.01 MGD; 0.02 MGD	38° 39' 16" N 77° 52' 32" W			



11. Sludge Treatment and Disposal Methods:

The sludge is aerobically stabilized and stored in a sludge holding tank. The stabilized and thickened sludge is transported to the Fauquier County Water and Sanitation Authority' Remington Regional Wastewater Treatment Facility (VA0076805) for ultimate processing and disposal.

12. Discharges and DEQ's Monitoring Stations within a 2-Mile Radius of Discharge Point

	TABLE 2						
WQM Station/VPDES Permit Number	Description						
3-BRW000.29	Barrows Run – DEQ Ambient Water Quality Monitoring Station, located at the Spring Drive Bridge, 0.29 river miles upstream from its confluences with the Rappahannock River. This station is not impacted by this discharge.						
3-GRT001.70	Great Run – DEQ Ambient Water Quality Monitoring Station, located at the Route 687 Bridge This station is not impacted by this discharge.						
VA0080527	VPDES Permit for the Clevengers Village WWTP (0.9 MGD Design Flow). The discharge is approximately 0.39 river miles upstream from this discharge.						

13. Material Storage:

TABLE 3 - Material Storage							
Materials Description	Materials Description Volume Stored Spill/Stormwater Prevention Measures						
Soda Ash 2- 50 lbs bags Storage/Lab Building							

14. Site Inspection:

Performed by Joan Crowther on December 3, 2013 (see Attachment 3).

15. Receiving Stream Water Quality and Water Quality Standards:

a. Ambient Water Quality Data

Outfall 001 discharges to a segment of the Rappahannock River that has not been monitored or assessed by DEQ.

The nearest downstream segment of the Rappahannock River that was assessed in the Virginia's 2012 Integrated Report (IR) is located approximately 7.8 miles downstream of Outfall 001. The following DEQ monitoring stations are located in this segment:

- 1) 3-RPP150.32, at Route 621 (ambient water quality) and
- 2) 3-RPP150.20, downstream of Route 621 (freshwater probabilistic).

DEQ benthic macroinvertebrate biological monitoring and associated chemical data finds this segment to be fully supporting the aquatic life and wildlife uses. The fish consumption use is fully supporting based on water column metals data.

E. coli monitoring find a bacterial impairment, resulting in an impaired classification for the recreation use. This impairment is nested within the downstream completed bacteria TMDL for the Rappahannock River.

b. 303(d) Listed Downstream Segments and Total Maximum Daily Loads (TMDLs)

				TABLE 4		•	
Impairment Information in the Draft 2012 Integrated Report							
Waterbody Name	Impaired Use	Cause	Distance From Outfall	TMDL completed	WLA	Basis for WLA	TMDL Schedule
Rappahannock River	Recreation	E. coli	3.8 miles	Rappahannock River Basin Bacteria 01/23/2008	3.48E+10 cfu/year <i>E. coli</i>	126 cfu/100ml E. coli 0.02 MGD	

The Planning Statement dated August 6, 2013, can be found as Attachment 4.

c. Receiving Stream Water Quality Criteria

Part IX of 9VAC25-260 (360-550) designates classes and special standards applicable to defined Virginia river basins and sections. The receiving stream, Rappahannock River, is located within Section 3 of the Rappahannock River Basin, and classified as a Class III water.

At all times, Class III waters must achieve a dissolved oxygen (D.O.) of 4.0 mg/L or greater, a daily average D.O. of 5.0 mg/L or greater, a temperature that does not exceed 32°C, and maintain a pH of 6.0-9.0 standard units (S.U.).

The Freshwater Water Quality/Wasteload Allocation Analysis (Attachment 5) details other water quality criteria applicable to the receiving stream.

Some Water Quality Criteria are dependent on the temperature and pH and Total Hardness of the stream and final effluent. The stream and final effluent values used for part of Attachment 5 are as follows:

pH and Temperature for Ammonia Criteria:

The freshwater, aquatic life Water Quality Criteria for Ammonia are dependent on the instream temperature and pH. Since the effluent may have an impact on the instream values, the temperature and pH values of the effluent must also be considered when determining the ammonia criteria for the receiving stream. The 90th percentile temperature and pH values are used because they best represent the critical design conditions of the receiving stream.

Staff has re-evaluated/reviewed the receiving stream ambient monitoring data and the effluent data for pH and temperature. The receiving stream pH and temperature values were determined by using the DEQ ambient water quality data for the VAN-E20R waterbody for the period of February 1999 through August 2010.

TABLE 5								
Parameter	90 th Percentile Annual	10 th Percentile	90 th Percentile Wet	10 th Percentile Wet				
Temperature (°C)	23.4		_14.8					
pH (SU)	7.0	6.2	7.3	6.5				

The effluent pH and temperature data were determined by using the daily effluent results from November 2011 through October 2013. This timeframe was selected because the "new" wastewater treatment plant was in operation and this time period demonstrated the treatment efficiency for the new plant. Certificate to Operate was issued on October 6, 2011.

TABLE 6					
Parameter	90 th Percentile Annual	10 th Percentile			
Temperature (°C)	26.9				
pH (SU)	8.3	7.3			

The effluent data are presented in Attachment 6.

Total Hardness for Hardness-Dependent Metals Criteria:

The Water Quality Criteria for some metals are dependent on the receiving stream's total hardness (expressed as mg/L calcium carbonate) as well as the total hardness of the final effluent.

The receiving stream total hardness data was determined by using the DEQ ambient water quality data for the VAN-E20R waterbody for the period of February 1999 through August 2010. The total hardness calculated for this waterbody was 44.2 mg/L.

There is no hardness data for this facility. Staff guidance suggests using a default hardness value of 50 mg/L CaCO3 for streams east of the Blue Ridge.

The hardness-dependent metals criteria in Attachment 5 are based on this default value.

Bacteria Criteria:

The Virginia Water Quality Standards at 9VAC25-260-170A state that the following criteria shall apply to protect primary recreational uses in surface waters:

E. coli bacteria per 100 ml of water shall not exceed a monthly geometric mean of 126 n/100 mls for a minimum of four weekly samples taken during any calendar month.

d. Receiving Stream Special Standards

The State Water Control Board's Water Quality Standards, River Basin Section Tables (9VAC25-260-360, 370 and 380) designates the river basins, sections, classes, and special standards for surface waters of the Commonwealth of Virginia. The receiving stream, Rappahannock River, is located within Section 3 of the Rappahannock River Basin. There are no special standards for this section.

e. Threatened or Endangered Species

The Virginia DGIF Fish and Wildlife Information System Database was searched on July 29, 2013 for records to determine if

there are threatened or endangered species in the vicinity of the discharge. Lasmigona sbuviridis, Floater green, was identified within a 2 mile radius of the discharge. It is listed as a State threatened species. DGIF was coordinated with on July 29, 2013 for their comments regarding this reissuance. By email dated August 22, 2013 (Attachment 7), DGIF responded by stating:

According to our records, the Rappahannock River is a designated Threatened and Endangered (T&E) species water for the state Threatened (ST) green floater mussel. It is also predicted habitat for the federal Endangered state Endangered (FESE) dwarf wedgemussel.

In order to protect aquatic resources, we generally recommend ultraviolet (UV) disinfection rather than chlorination disinfection. If chlorination becomes necessary and is used, we recommend and support continued dechlorination, prior to discharge. The ammonia limits proposed within the EPA rule are expressed on the basis of total ammonia-nitrogen (TAN). The proposed EPA ammonia limit for waters with mussels (not T&E mussels, any mussel species) is:

- CMC (Criterion Maximum Concentration or acute) 2.9 mg N/L (at pH 8 and 25C)
- CCC (Criterion Continuous Concentration or chronic) 0.26 mg N//L (at pH 8 and 25C) with a 4-day average within the 30 day average period no higher than 2.5 the CCC, which would be 0.65 mg N/L.

The ammonia limits proposed within the EPA rule are the best information currently available regarding ammonia levels protective of mussels. Therefore, we recommend and support the EPA values being implemented in this permit for this and all future VPDES permits.

The wastewater treatment plant has been disinfecting with UV since its installation of the new wastewater treatment in October 2011. DEQ has reviewed DGIF's comments and at this time no change to the draft permit are proposed. The limits proposed in this draft permit are protective of the Virginia Water Quality Standards and protect the threatened and endangered species found near the discharge.

The stream that the facility discharges to is within a reach identified as having an Anadromous Fish Use. It is staff's best professional judgment that the proposed limits are protective of this use.

16. Antidegradation (9VAC25-260-30):

All state surface waters are provided one of three levels of antidegradation protection. For Tier 1 or existing use protection, existing uses of the water body and the water quality to protect these uses must be maintained. Tier 2 water bodies have water quality that is better than the water quality standards. Significant lowering of the water quality of Tier 2 waters is not allowed without an evaluation of the economic and social impacts. Tier 3 water bodies are exceptional waters and are so designated by regulatory amendment. The antidegradation policy prohibits new or expanded discharges into exceptional waters.

The receiving stream has been classified as Tier 2. This segment of the Rappahannock River was classified as Tier 2 in 1997 and has been carried forward with each reissuance since then. No significant degradation to the existing water quality will be allowed. In accordance with current DEQ guidance, no significant lowering of water quality is to occur where permit limits are based on the following:

- The dissolved oxygen in the receiving stream is not lowered more than 0.2 mg/L from the existing levels;
- The pH of the receiving stream is maintained within the range 6.0-9.0 S.U.;
- There is compliance with all temperature criteria applicable to the receiving stream;
- No more than 25% of the unused assimilative capacity is allocated for toxic criteria established for the protection of aquatic life; and
- No more than 10% of the unused assimilative capacity is allocated for criteria for the protection of human health.

The antidegradation policy also prohibits the expansion of mixing zones to Tier 2 waters unless the requirements of 9VAC25-260-30.A.2 are met. The draft permit is not proposing an expansion of the existing mixing zone.

17. Effluent Screening, Wasteload Allocation, and Effluent Limitation Development:

To determine water quality-based effluent limitations for a discharge, the suitability of data must first be determined. Data is suitable for analysis if one or more representative data points is equal to or above the quantification level ("QL") and the data represent the exact pollutant being evaluated.

Next, the appropriate Water Quality Standards are determined for the pollutants in the effluent. Then, the Wasteload Allocations (WLA) are calculated. The WLA values are then compared with available effluent data to determine the need for effluent limitations. Effluent limitations are needed if the 97th percentile of the daily effluent concentration values is greater than the acute wasteload allocation or if the 97th percentile of the four-day average effluent concentration values is greater than the chronic wasteload allocation. Effluent limitations are the calculated on the most limiting WLA, the required sampling frequency, and statistical characteristics of the effluent data.

a. Effluent Screening:

Effluent data obtained from the facility's DMRs November 2011 to October 2013 have been reviewed and determined to be suitable for evaluation. The following exceedances were reported:

June 2012 – pH July 2012 – Dissolved Oxygen October 2012 – Dissolved Oxygen January 2013 – E.coli Bacteria

The following pollutants require a wasteload allocation analysis: Ammonia as N.

b. Mixing Zones and Wasteload Allocations (WLAs):

Wasteload allocations (WLAs) are calculated for those parameters in the effluent with the reasonable potential to cause an exceedance of water quality criteria. The basic calculation for establishing a WLA is the steady state complete mix equation:

	WLA	$= \frac{\text{Co} \left[\text{Qe} + (\text{f}) (\text{Qs}) \right] - \left[(\text{Cs}) (\text{f}) (\text{Qs}) \right]}{\text{Qe}}$
Where:	WLA	= Wasteload allocation
	Co	= In-stream water quality criteria
•	Qe	= Design flow
	\mathbf{f}	 Decimal fraction of critical flow from mixing evaluation
	Qs	= Critical receiving stream flow
	`	(1Q10 for acute aquatic life criteria; 7Q10 for chronic aquatic life criteria; 30Q10 for ammonia criteria; harmonic mean for carcinogen-human health criteria; and 30Q5 for non-carcinogen human health criteria)
	Cs	= Mean background concentration of parameter in the receiving stream.

The Water Quality Standards contain two distinct mixing zone requirements. The first requirement is general in nature and requires the "use of mixing zone concepts in evaluating permit limits for acute and chronic standards in 9VAC25-260-140.B". The second requirement is specific and establishes special restrictions for regulatory mixing zones "established by the Board".

The Department of Environmental Quality uses a simplified mixing model to estimate the amount of mixing of a discharge with the receiving stream within specified acute and chronic exposure periods. The simplified model contains the following assumptions and approximations:

- The effluent enters the stream from the bank, either via a pipe, channel or ditch.
- The effluent velocity isn't significantly greater (no more than 1 2 ft/sec greater) than the stream velocity.
- The receiving stream is much wider than its depth (width at least ten times the depth).
- Diffusive mixing in the longitudinal direction (lengthwise) is insignificant compared with advective transport (flow).
- Complete vertical mixing occurs instantaneously at the discharge point. This is assumed since the stream depth is much smaller than the stream width.
- Lateral mixing (across the width) is a linear function of distance downstream.
- The effluent is neutrally buoyant (e.g. the effluent discharge temperature and salinity are not significantly different from the stream's ambient temperature and salinity).
- Complete mix is determined as the point downstream where the variation in concentration is 20% or less across the
 width and depth of the stream.
- The velocity of passing and drifting organisms is assumed equal to the stream velocity.

If it is suitably demonstrated that a reasonable potential for lethality or chronic impacts within the physical mixing area doesn't exist, then the basic complete mix equation, with 100% of the applicable stream flow, is appropriate. If the mixing analysis

determines there is a potential for lethality or chronic impacts within the physical mixing area, then the proportion of stream flow that has mixed with the effluent over the allowed exposure time is used in the basic complete mix equation. As such, the wasteload allocation equation is modified to account for the decimal fraction of critical flow (f).

Staff derived wasteload allocations where parameters are reasonably expected to be present in an effluent (e.g., total residual chlorine where chlorine is used as a means of disinfection) and where effluent data indicate the pollutant is present in the discharge above quantifiable levels. With regard to the Outfall 001 discharge, ammonia as N is likely present since this is a WWTP treating sewage. As such, Attachment 8 details the mixing analysis results and WLA derivations for these pollutants.

Antidegradation Wasteload Allocations (AWLAs).

Since the receiving stream has been determined to be a Tier II water, staff must also determine antidegradation wasteload allocations (AWLAs). The steady state complete mix equation is used substituting the antidegradation baseline (Cb) for the instream water quality criteria (Co):

$$AWLA = \frac{Cb(Qe + Qs) - (Cs)(Qs)}{Qe}$$

Where: AWLA = Antidegradation-based wasteload allocation

Cb = In-stream antidegradation baseline concentration

Qe = Design flow

Qs = Critical receiving stream flow

(1Q10 for acute aquatic life criteria; 7Q10 for chronic aquatic life criteria; 30Q10 for ammonia criteria; harmonic mean for carcinogen-human health

criteria; and 30Q5 for non-carcinogen human health criteria)

Cs = Mean background concentration of parameter in the receiving stream.

Calculated AWLAs for the pollutants noted in b. above are presented in Attachment 5.

c. Effluent Limitations Toxic Pollutants, Outfall 001:

9VAC25-31-220.D. requires limits be imposed where a discharge has a reasonable potential to cause or contribute to an instream excursion of water quality criteria. Those parameters with AWLAs that are near effluent concentrations are evaluated for limits.

The VPDES Permit Regulation at 9VAC25-31-230.D requires that monthly and weekly average limitations be imposed for continuous discharges from POTWs and monthly average and daily maximum limitations be imposed for all other continuous non-POTW discharges.

1) Ammonia as N:

In the 1993 permit reissuance, Ammonia as N effluent limitation for the 0.01743 MGD design flow was established as 15.4 mg/L monthly average and daily maximum. Documentation for this Ammonia as N effluent limitation is found in Attachment 9.

In the 2003 permit reissuance, the Ammonia as N effluent limitations were again reviewed and 15.6 mg/L monthly average and 23.4 mg/L daily maximum were established. The following documentation was the basis for the Ammonia as N effluent limitations.

Ambient water quality pH and temperature data used to derive the criteria were available from STORET for monitoring station 3-RPP147.10 and are presented in Attachment 10. The 90th percentile pH value of 7.7 SU, and the 90th percentile temperature of 24.1°C were obtained. Staff re-evaluated the receiving stream ambient monitoring data for pH and temperature and found no significant differences from the data used to establish ammonia criteria and subsequent effluent limits in the 1998 permit. Therefore, the previously established criteria were carried forward in the 2003 reissuance process.

		TABLE 7						
90th Percentile Comparison								
Season	1998 90 th Percentile pH	2003 90 th Percentile pH	1998 90 th Percentile Temperature	2003 90 th Percentile Temperature				
Year Round	7.8	7.7	24.7°C	24.1°C				

Antidegradation baseline was set for ammonia because it is present in sewage and had a reasonable potential to violate water quality criteria

The formula for determining the baseline is:

Baseline = $c_s + (0.25)$ (criteria - c_s), where c_s = background stream concentration.

The background concentration for ammonia was assumed to be 0.0 mg/L.

TABLE 8 - Antidegradation Baselines and WQ Based Criteria (Attachment 10)							
	WQ Base	d Criteria	Antidegra	radation Baseline			
Ammonia as N	Acute	Chronic	Acute	Chronic			
(mg/L)	7.80	1.78	1.95	0.44			

The antidegradation policy also prohibits the expansion of mixing zones to Tier 2 waters unless the requirements of 9 VAC 25-260-30.A.2. are met. The draft permit is not proposing an expansion of the existing mixing zone. The mixing zone analysis documentation was for the 2003 permit reissuance are in Attachment 10. The mixing zone predications were as follows:

- > A complete mix assumption is appropriate for this situation providing no more than 9.27% of the 1Q10 was used.
- > A complete mix assumption is appropriate in this situation and the entire 7Q10 or entire 30Q10 may be used.

Calculated AWLAs for the pollutants are summarized below. The most stringent WLAs were used to develop the permit limits.

TABLE 9 - Comparison of WLAs							
	Water	Quality I	Based WLAs	Antidegra	dation WLAs		
Ammonia as N (mg/L)	Ac	ute	Chronic	Acute	Chronic		
\	59.24	15.6*	151.19	140.67	37.80		

*For stream dominated dischargers (defined as having an Instream Waste Concentration (IWC) of 50% or less at critical conditions), a steady state complete mix equation could result in a relatively large acute WLA. Discharges containing this large acute WLA could result in an introduction of concentrations of pollutants into the receiving stream that would not completely mix in a rapid manner and may possibly cause lethality in the allocated impact zone. In order to ensure protection against lethality, the acute WLA for discharges into stream dominated situations are set at two times the acute standard. Therefore, the acute WLA for ammonia was calculated as:

$$(7.80 \text{ mg/L}) (2) = 15.6 \text{ mg/L}$$

The weekly average value of 23.4 mg/L was determined by multiplying the monthly average value (15.6 mg/L) by a 1.5 factor.

DEQ guidance suggests using a sole data point of 9.0 mg/L for discharges containing domestic sewage to ensure the evaluation adequately addresses the potential for Ammonia as N to be present in the discharge containing domestic sewage. During the 2008 permit reissuance, the Ammonia as N monthly average was rounded from 15.6 mg/L to 16 mg/L and the weekly maximum was corrected. The practice of multiplying the monthly average by 1.5 to determine the weekly maximum was no longer done. The monthly average and weekly maximum effluent limitations for toxic parameters are the same value; therefore, during the 2008 permit reissuance the Ammonia as N weekly average was changed to 16 mg/L. It is staff's best professional judgment that the existing Ammonia as N effluent limitations are still appropriate and will be carried forward in this permit reissuance. See Attachment 10 for the Ammonia as N statistical calculations.

3) Metals/Organics:

No metals or organics data were available for review; therefore, no effluent limits are proposed.

d. Effluent Limitations and Monitoring, Outfall 001 - Conventional and Non-Conventional Pollutants

No changes to dissolved oxygen (D.O.), biochemical oxygen demand-5 day (BOD₅), total suspended solids (TSS), *E. coli* Bacteria, and pH limitations are proposed.

Dissolved Oxygen and BOD₅ limitations are based on the stream modeling conducted in January 1988 and July 1998 (Attachment 11) and are set to ensure that the receiving stream D.O. does not decrease more than 0.2 mg/l to meet the requirements of the antidegradation policy.

It is staff's practice to equate the Total Suspended Solids limits with the BOD₅ limits. TSS limits are established to equal BOD₅ limits since the two pollutants are closely related in terms of treatment of domestic sewage. The limit for Total Suspended Solids is based on Best Professional Judgment.

pH limitations are set at the water quality criteria.

E. coli limitations are in accordance with the Water Quality Standards 9VAC25-260-170.

e. Effluent Limitations and Monitoring Summary:

The effluent limitations are presented in the following table. Limits were established for Flow, BOD₅, Total Suspended Solids, Ammonia as N, pH, and Dissolved Oxygen.

The mass loading (kg/d) for monthly and weekly averages were calculated by multiplying the concentration values (mg/L), with the flow values (in MGD) and a conversion factor of 3.785.

Sample Type and Frequency are in accordance with the recommendations in the VPDES Permit Manual (2010).

The VPDES Permit Regulation at 9VAC25-31-30 and 40 CFR Part 133 require that the facility achieve at least 85% removal for BOD and TSS (or 65% for equivalent to secondary). The limits in this permit are water-quality-based effluent limits and result in greater than 85% removal.

18. Antibacksliding:

All limits in this permit are at least as stringent as those previously established. Backsliding does not apply to this reissuance.

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19.A. Effluent Limitations/Monitoring Requirements:

Design flow is 0.01 MGD.

Effective Dates: During the period beginning with the permit's effective date and lasting until the issuance of the CTO for the 0.02

MGD facility or the permit's expiration date, whichever comes first.

PARAMETER	BASIS FOR	DI	MONITORING REQUIREMENTS				
	LIMITS	Monthly Average	Weekly Average	Minimum	Maximum	Frequency	Sample Type
Flow (MGD)	NA	NL	NA	NA	NL	1/D	Estimated
pН	3	NA	NA	6.0 S.U.	9.0 S.U.	1/D	Grab
BOD ₅	3,5	30 mg/L 1.1 kg/day	45 mg/L 1.7 kg/day	NA NA		1/M	Grab
Total Suspended Solids (TSS)	2	30 mg/L 1.1 kg/day	45 mg/L 1.7 kg/day	NA	NA	1/M	Grab
Dissolved Oxygen (DO)	3	NA	NA	6.0 mg/L	NA	1/D	Grab
Ammonia, as N (mg/L)	3,5	16	16	NA	NA	1/M	Grab
E. coli (Geometric Mean)(a)	3	126 n/100mls	NA	NA	NA	1/W	Grab

The basis for the limitations codes are:

MGD = Million gallons per day.

1/D = Once every day.

1. Federal Effluent Requirements

NA = Not applicable.

1/M = Once every month.

2. Best Professional Judgment

NL = No limit; monitor and report.

1/W = Once every week.

3. Water Quality Standards

S.U. = Standard units.

4. DEQ Disinfection Guidance

5. Stream Model- Attachment 11

Estimated = Reported flow is to be based on the technical evaluation of the sources contributing to the discharge

Grab = An individual sample collected over a period of time not to exceed 15 minutes.

(a) = Between 10 AM and 4 PM.

B. Effluent Limitations/Monitoring Requirements:

Design flow is 0.02 MGD.

Effective Dates: During the period beginning with the issuance of the CTO for the 0.02 MGD facility and lasting until the

permit's expiration date.

PARAMETER	BASIS FOR	DI	DISCHARGE LIMITATIONS									
	LIMITS	Monthly Average	Weekly Average	Minimum	Maximum	Frequency	Sample Type Estimated					
Flow (MGD)	NA	NL	NA	NA	NL	1/D						
pH	3	NA	NA	6.0 S.U.	9.0 S.U.	1/D	Grab					
BOD ₅	3,5	30 mg/L 2.3 kg/day	45 mg/L 3.4 kg/day	NA	NA	1/M	Grab					
Total Suspended Solids (TSS)	2	30 mg/L 2.3 kg/day	45 mg/L 3.4 kg/day	NA	NA	1/M	Grab					
Dissolved Oxygen (DO)	3	NA	NA	6.0 mg/L	NA	1/D	Grab					
Ammonia, as N (mg/L)	3,5	16	16	NA	NA	1/M	Grab					
E. coli (Geometric Mean)(a)	3	126 n/100mls	NA	NA NA NA		1/W	Grab					

The basis for the limitations codes are:

MGD = Million gallons per day.

1/D = Once every day.

I. Federal Effluent Requirements

NA = Not applicable.

1/M = Once every month.

2. Best Professional Judgment

NL = No limit; monitor and report.

1/W = Once every week.

3. Water Quality Standards

S.U. = Standard units.

4. DEQ Disinfection Guidance

5. Stream Model- Attachment 11

Estimated = Reported flow is to be based on the technical evaluation of the sources contributing to the discharge

Grab = An individual sample collected over a period of time not to exceed 15 minutes.

(a) = Between 10 AM and 4 PM.

C. Groundwater Monitoring Requirements:

Effective Dates: During the period beginning with the permit's effective date and lasting until the permit

expiration date.

For wells: MW1, MW3 and MW4

	** **	T * *4	Monitoring 1	Requirements
Parameters	Units	Limit	Frequency	Sample Type
Static water level	Ft.	NL	1/3M	Measured
pН	S.U.	NL	1/3M	Grab
Conductivity	μmho/cm	NL	1/3M	Grab
Total Organic Carbon	mg/L	NL	1/3 M	Grab
Total Dissolved Solids	mg/L	NL	1/3M	Grab
Ammonia as N	mg/L	NL	1/3 M	Grab
Temperature	deg C	NL	1/3 M	IS

- 1. Sampling shall be conducted quarterly and reported quarterly. The quarterly reporting periods shall be January, April, July, and October. The DMR shall be submitted no later than the 10th day of the month following the monitoring period.
- 2. The permittee may request in writing that the sampling frequency be reduced or eliminated after one year of monitoring.
- 3. The static water level shall be measured prior to bailing the well water for sampling. At least three volumes of groundwater shall be withdrawn immediately before sampling each well.
 - 1/3M = Once per quarter.
 - IS = Immersion Stabilization
 - Grab = An individual sample collected over a period not to exceed 15-minutes.

20. Other Permit Requirements:

a. Part I.B. of the permit contains quantification levels and compliance reporting instructions.

9VAC25-31-190.L.4.c. requires an arithmetic mean for measurement averaging and 9VAC25-31-220.D requires limits be imposed where a discharge has a reasonable potential to cause or contribute to an in-stream excursion of water quality criteria. Specific analytical methodologies for toxics are listed in this permit section as well as quantification levels (QLs) necessary to demonstrate compliance with applicable permit limitations or for use in future evaluations to determine if the pollutant has reasonable potential to cause or contribute to a violation. Required averaging methodologies are also specified.

21. Other Special Conditions:

- a. 95% Capacity Reopener. The VPDES Permit Regulation at 9VAC25-31-200.B.4 requires all POTWs and PVOTWs develop and submit a plan of action to DEQ when the monthly average influent flow to their sewage treatment plant reaches 95% or more of the design capacity authorized in the permit for each month of any three consecutive month period. The facility is a PVOTW.
- b. Indirect Dischargers. Required by VPDES Permit Regulation, 9VAC25-31-200 B.1 and B.2 for POTWs and PVOTWs that receive waste from someone other than the owner of the treatment works.
- c. O&M Manual Requirement. Required by Code of Virginia §62.1-44.19; Sewage Collection and Treatment Regulations, 9VAC25-790; VPDES Permit Regulation, 9VAC25-31-190.E. The permittee shall maintain a current Operations and Maintenance (O&M) Manual. The permittee shall operate the treatment works in accordance with the O&M Manual and shall make the O&M Manual available to Department personnel for review upon request. Any changes in the practices and procedures followed by the permittee shall be documented in the O&M Manual within 90 days of the effective date of the changes. Non-compliance with the O&M Manual shall be deemed a violation of the permit.
- d. CTC, CTO Requirement. The Code of Virginia § 62.1-44.19; Sewage Collection and Treatment Regulations, 9VAC25-790 requires that all treatment works treating wastewater obtain a Certificate to Construct prior to commencing construction and to obtain a Certificate to Operate prior to commencing operation of the treatment works.

- e. Licensed Operator Requirement. The Code of Virginia at §54.1-2300 et seq. and the VPDES Permit Regulation at 9VAC25-31-200 C, and by the Board for Waterworks and Wastewater Works Operators and Onsite Sewage System Professionals Regulations (18VAC160-20-10 et seq.) requires licensure of operators. This facility requires a Class IV operator.
- f. Reliability Class. The Sewage Collection and Treatment Regulations at 9VAC25-790 require sewage treatment works to achieve a certain level of reliability in order to protect water quality and public health consequences in the event of component or system failure. Reliability means a measure of the ability of the treatment works to perform its designated function without failure or interruption of service. The facility is required to meet a Reliability Class of II.
- g. Sludge Reopener. The VPDES Permit Regulation at 9VAC25-31-220.C requires all permits issued to treatment works treating domestic sewage (including sludge-only facilities) include a reopener clause allowing incorporation of any applicable standard for sewage sludge use or disposal promulgated under Section 405(d) of the CWA. The facility includes a sewage treatment works.
- h. Sludge Use and Disposal. The VPDES Permit Regulation at 9VAC25-31-100.P; 220.B.2, and 420 through 720, and 40 CFR Part 503 require all treatment works treating domestic sewage to submit information on their sludge use and disposal practices and to meet specified standards for sludge use and disposal. The facility includes a treatment works treating domestic sewage.
- i. TMDL Reopener. This special condition is to allow the permit to reopened if necessary to bring it in compliance with any applicable TMDL that may be developed and approved for the receiving stream.
- j. **Groundwater Monitoring.** This special condition requires the pemittee to continue the groundwater monitoring in accordance with the *Protocol for Groundwater Sampling* contained in the "Fauquier Springs Country Club Wastewater Treatment Plant Updated Groundwater Monitoring Plan dated May 2008 and P.E. dated May 19, 2009".
- k. Financial Assurance. This permittee is required by Code of Virginia §62.1.-44.18:3 and the Board's Financial Assurance Regulation, 9VAC25-650-1, et seq. to submit a closure plan and maintain adequate financial assurance in the event the facility ceases operations. This regulation is applicable to owners and operators of PVOTWs with a design flow >0.0001 MGD but <0.040 MGD and treating sewage from private residences. The permitted facility is a PVOTW with a design flow of 0.01 MGD with an additional design flow tier of 0.02 MGD, and treats sewage generated from three private residences.
- 1. Treatment Works Closure Plan. The State Water Control Law §62.1-44.15:1.1, makes it illegal for an owner to cease operation and fail to implement a closure plan when failure to implement the plan would result in harm to human health or the environment. This condition is used to notify the owner of the need for a closure plan where a facility is being replaced or is expected to close.

22. Permit Section Part II.

Part II of the permit contains standard conditions that appear in all VPDES Permits. In general, these standard conditions address the responsibilities of the permittee, reporting requirements, testing procedures and records retention.

23. Changes to the Permit from the Previously Issued Permit:

- a. Special Conditions:
 - 1. The Groundwater Corrective Action Plan Special Condition was removed since the permittee replaced the lagoon wastewater treatment plant with a 0.01 MGD extended aeration package plant.
 - 2. Financial Assurance and Treatment Works Closure Plan special conditions were added because three residential homes are being provided sanitary sewer treatment by this wastewater treatment plant and this plant is privately owned. (9 VAC 25-650).
- b. Monitoring and Effluent Limitations:
 - 1. The Total Residual Chlorine effluent limitations and monitoring were removed due to the UV Disinfection installation.
 - 2. The E. coli's frequency of analysis was increased in accordance with the VPDES Permit Manual (2010) and the Virginia Water Quality Standards.
 - 3. The Effluent Limitations/Monitoring Requirement page for the 0.02 MGD lagoon wastewater treatment plant was removed since this plant was replaced with a 0.01 MGD extended aeration package plant. The lagoon was properly abandoned.
 - 4. The Groundwater Monitoring Requirements were modified as follows: 1) E. coli bacteria monitoring was eliminated; 2)

Nitrite-N monitoring was eliminated; 3) Nitrate-N monitoring was eliminated; 4) the remaining parameters are the same except the frequency of monitoring was reduced from monthly to quarterly.

23. Variances/Alternate Limits or Conditions:

There are no variances / alternate limits or conditions in this draft permit.

25. Public Notice Information:

First Public Notice Date: 2/12/14 Second Public Notice Date:

2/19/14

Public Notice Information is required by 9VAC25-31-280 B. All pertinent information is on file and may be inspected, and copied by contacting the: DEQ Northern Regional Office, 13901 Crown Court, Woodbridge, VA 22193, Telephone No. (703) 583-3925, joan crowther@deq.virginia.gov. See Attachment 12 for a copy of the public notice document.

Persons may comment in writing or by email to the DEQ on the proposed permit action, and may request a public hearing, during the comment period. Comments shall include the name, address, and telephone number of the writer and of all persons represented by the commenter/requester, and shall contain a complete, concise statement of the factual basis for comments. Only those comments received within this period will be considered. The DEQ may decide to hold a public hearing, including another comment period, if public response is significant and there are substantial, disputed issues relevant to the permit. Requests for public hearings shall state 1) the reason why a hearing is requested; 2) a brief, informal statement regarding the nature and extent of the interest of the requester or of those represented by the requester, including how and to what extent such interest would be directly and adversely affected by the permit; and 3) specific references, where possible, to terms and conditions of the permit with suggested revisions. Following the comment period, the Board will make a determination regarding the proposed permit action. This determination will become effective, unless the DEQ grants a public hearing. Due notice of any public hearing will be given. The public may request an electronic copy of the draft permit and fact sheet or review the draft permit and application at the DEQ Northern Regional Office by appointment.

26. Additional Comments:

Previous Board Action(s): None.

Staff Comments: After the public comment period had closed, staff became aware that this wastewater treatment plant was providing sanitary sewerage service to three residential homes. It was learned that one of these homes had been connected to the plant in 1960s and the other two homes were connected ~2004. Because this is a privately owned wastewater treatment plant and the design flows are greater than 0.001 MGD and less than 0.04 MGD, the Closure Plans and Demonstration of Financial Capability Requirement Regulation (9 VAC 25-650) must be complied with. Therefore, the reissuance was delayed so that this regulation's requirements could be addressed and complied with. The Financial Assurance was signed off by DEQ-CO on October 29, 2014. DEQ-NRO was notified on November 4, 2014 that all financial assurance requirements had been completed.

Public Comment: 1) DGIF requested to review this permit in accordance with the VPDES Memorandum of Understanding dated April 16, 2007. See Section 15.e of this fact sheet for their comments.

2) No comments were received during the public comment period.

Attachment Number	Description of Attachment
1	1997 Flow Frequency Determination
2	Certificate to Operate dated October 6, 2011
3	Site Inspection
4	Planning Statement dated August 6, 2013
5	Freshwater Water Quality/Wasteload Allocation Analysis dated January 6, 2014
6	Effluent Data November 2011 through October 2013
7	DGIF Comments dated August 22, 2013
8	2014 Mixing Analysis Results
9	1993 Ammonia as N Calculation Documentation
10	2003 Ammonia as N Calculation Documentation
11	Stream Models – January 1988, July 1998
12	Public Notice

MEMORANDUM

DEPARTMENT OF ENVIRONMENTAL QUALITY - WATER DIVISION

Water Quality Assessments and Planning

629 E. Main Street P.O. Box 10009 Richmond, Virginia 23240

SUBJECT: Flow Frequency Determination

Fauguier Springs Country Club STP - VA#0077411

TO: James A. Olson, NRO

FROM: Paul E. Herman, P.E., WQAP

DATE: November 4, 1997

COPIES: Ron Gregory, Charles Martin, File

This memo supercedes my February 9, 1993 memo to Joan Crowther concerning flow frequencies for the subject facility.

The Fauquier Springs Country Club STP discharges to the Rappahannock River near the Route 802 bridge in Fauquier County, VA. Stream flow frequencies are required at this site for use by the permit writer in developing effluent limitations for the VPDES permit.

The USGS operated a continuous record gage on the Rappahannock River near Warrenton, VA (#01662000) from 1943 to 1986. The gage was located approximately 10 miles upstream from the discharge point. The flow frequencies for the gage and the discharge point are presented below. The values at the discharge point were determined by drainage area proportions and do not address any withdrawals, discharges, or springs lying upstream.

Rappahannock River near Warrenton, VA (#01662000):

Rappahannock River at discharge point:

Drainage Area = 205.7 mi

1Q10 = 2.2 cfs 142 M6D High Flow 1Q10 = 26 cfs 16.8 mgd

7Q10 = 2.6 cfs 1.68 meD High Flow 7Q10 = 33 cfs al.3 mgd

30Q5 = 9.6 cfs 6.2 meD HM = 39 cfs a5.2 mgd

30Q10 = 5.5 cfs 3.6 msd Highflow 30Q10 = 47 cfs 30.4 msd

The high flow months are December through May. If you have any questions concerning this analysis, please let me know.



COMMONWEALTH of VIRGINIA

DEPARTMENT OF ENVIRONMENTAL QUALITY NORTHERN REGIONAL OFFICE

Douglas W. Domenech Secretary of Natural Resources 13901 Crown Court, Woodbridge, Virginia 22193 (703) 583-3800 Fax (703) 583-3821 www.deq.virginia.gov

David K. Paylor Director

Thomas A. Faha Regional Director

October 6, 2011

Fauquier County Fauquier Springs CC WWTP Replacement PTL#25369, Permit VA0077411

Mr. William Fendley Sulphur Springs Investment Corp 9236 Tournament Drive Warrenton, VA 22186

Dear Mr. Fendley:

In accordance with 9VAC25-790-190 of the Commonwealth of Virginia's Sewage Collection and Treatment Regulations, this letter transmits the Certificate to Operate (CTO) for Fauquier Springs Country Club WWTP Replacement located in Fauquier County. The CTO is being issued based on the Application for Certificate to Operate dated August 22, 2011, and received by this office on August 23, 2011.

Please be advised that in accordance with your VPDES Permit VA0077411 Part I.C.3., an updated O&M Manual shall be submitted within 90 days of the issuance of the CTO.

On October 5, 2011, I spoke with Don Hearl from ESS who operates the treatment plant regarding the Closure Plan for the old wastewater lagoon. Based on my conversation with Mr. Hearl, DEQ understands that there will be no further discharge from the old wastewater lagoon and that any further dewatering will be processed through the new WWTP. If there is an emergency situation that will require the lagoon to discharge, you shall notify DEQ of the situation and provide a description of the reasoning for the discharge. In addition, the discharge from the lagoon shall be monitored on a weekly basis for TSS, BOD, and Ammonia as N until such time that the discharge ceases or the discharge from the lagoon no longer meets the permitted limits for one of the aforementioned parameters. This monitoring shall be in addition to the required monitoring for Outfall 001.

If you have any questions about this letter or the approval process, please contact me at (703)-583-3834 or alison thompson@deq.virginia.gov.

Respectfully,

Alison Thompson

Water Permits Technical Reviewer

ce:

VPDES Permit File VA0077411

VDH District Office, attn: Environmental Health Manager

Fauquier County Local Building Official

Earl Sutherland, Patton Harris Rust & Associates, 117 East Piccadilly St, Ste 200,

Winchester VA 226

Don Hearl, ESS

Attachment: CTO

Department of Environmental Quality

APPLICATION for CERTIFICATE TO OPERATE
Under the Sewage Collection and Treatment Regulations 9 VAC 25-790

	attachments. Form will expand as you enter information.
Project Title: (as it appears on plans) Fauguier Springs Cour	htry Club – Wastewater Treatment Plant Replacement
P.E. Seal Date on Cover: 1 April 2010	
Specifications Title and Date: Fauquier Springs Country Club	0 – Wastewater Treatment Plant Replacement, April 2010
Location of Project: SR 687 @ Rappahannock River	County/City: Fauguier County
Receiving Wastewater Collection System(s): NA	
Receiving Sewage Treatment Plant(s): NA	
PROJECT OWNER: Sulphur Springs Investment Corp.	PROJECT ENGINEER
Owner Contact Name: William Fendley	Name: Earl R. Sutherland, P. E.
Signature and Date:	Company Name: Patton Harris Rust & Associates
Address: 9236 Tournament Drive	Address:
Warrenion, Virginia 22186	117 East Piccadilly Street, Suite 200
Phone: 540.347.4025	Winchester, Virginia 22601
Email: info@fauquier springs.com	Phone: 540.667.2139 Email: esutherland@pennoni.com
PTL NUMBER FROM CERTIFICATE TO CONSTRUCT:	24868
Attach Copy of the original Certificate to Construct if issued	prior to November 9, 2008, or if a WQIF project. If applicable,
provide verification of compliance with any conditions in the (Profite to Construct
The state of the s	Sertificate to Constituet.
Design Sewage Flow: (a) average daily flow (MGD): 0.010	(b) peak flow (MGD): 0.015
, , , , , , , , , , , , , , , , , , , ,	(b) pour now (MOD)
For sewage treatment plant projects, provide the VPDES/VP.	A Permit Number: VA0077411
Is a new Discharge Monitoring Report (DMR) required? Yes	No 🛛
For Pump Stations and Sewage Treatment Plants check Reli	ability Class: I II 🛛 III
The following statement must be signed and sealed by the	te inspecting engineer: (DEO will not conduct a conferming
inspection.)	o mopeoung engineer. (DEQ will not conduct a confirming
"Ot-t-	
Statement of Completion:	
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I hereby certify that the construction work was confidence	d in accordance with the approved referenced design
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Inspections to certify the work." E.R. SUTHERLAN Lic. No. 5073 Inspecting Licensed Engineer's Signature and Original Salus For DEQ use only: In accordance with Code of Virginia 1950, as amended, Title of appropriate DEQ representative, serves as the Certificate to Compare the Compare of Environmental Quality Authorized Representative For sewage treatment plants, an Operation and Maintenance Manual must 790 and VPDES/VPA permit requirements. For pump stations, an Operation and Maintenance Manual must be maintained.	General Section 62.1-44.19, this form, signed by the operate for the referenced project. Section 62.1-44.19 CTO PTL Number
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Administrative Tracking Form for CTC Application

- Who must apply for a Certificate to Construct (CTC)?
 VAC 25-790-50 and 60 define who must apply for a CTC. In general, all new or expanded sewage treatment plant projects; major modifications of sewage treatment plants; gravity sewer projects with average day design flows over 40,000 gpd; and pump stations/force mains with average day design flows >2000 gpd must apply for a CTC.
- How long do you have to process the CTC?
 The CTC application is to be submitted at least 30 days prior to the desired start of construction. Either an email notice of an incomplete application or the approval must be processed within that time
- 3. Input the CTC application into the Plans Tracking Log as 'CTC Application'. See separate guidance on the PT log. The Log will generate a tracking number. That number is added to the submitted form by hand as the PTL number.

Project Name:	Fauquier Sprin	40 WWTP Improv
Date Received:	4-29-10	PTL#: 24868

4. Verify that all Information Requested on the Form is Provided:

Item	F F	Provided	1?	Notes
	Yes	No	N/A	
Project Title with Date (plans and spacs)	V	Lì	1 1	Specifications may be on the plans so not all projects have separate specs
Project Location	1	11	[]	Must have City/County
Receiving Systems Identified	1	i l	[]	Not applicable if this project owner owns the downstream collection and treatment
Contact Information	T XI	!	11	Must have
Project Description Attached	N	- 11	11	Must have
Letter of Acceptance	[!]	: 1	N	Must have for pump stations, collection systems, and satellite reclamation systems
Reliability Rating from VDH for Pump Stations only	[]	1	×	Need rating and statement of how meeting the rating
Design Sewage Flows	N	11	[]	Must have
Project Components checked	N	- 11	11	Must have
VPDES/VPA Permit Referenced	15	11	11	Must have for sewage treatment plants
Loan/Grant status	11	í Ì	×	WQIF projects cannot utilize this abbreviated process. Return the project.
Professional Engineer signature and seal	N	!]	11	Must have
Design exceptions noted?	li	i 1	11/	If yes, must have attached.

Note missing items and send email to project owner and engineer.

Log of telephone conversations and additional items received:

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FAUQUIER SPRINGS COUNTRY CLUB

WASTEWATER TREATMENT PLANT UPGRADE PROJECT

PROJECT DESCRIPTION

The project consists of the replacement of an existing 20,000 GPD aerated lagoon with a 10,000 GPD extended aeration treatment facility. The new treatment works will be located on the same site as the existing treatment facility and will discharge through the same outfall line. The treatment works will include coarse screening, flow equalization, biological treatment (extended aeration variant of the activated sludge process), and clarification. The existing chlorination/dechlorination facilities, cascade aeration, and outfall line will remain in service.

The process will also include an aerated biosolids stabilization and holding tank. The stabilized and thickened sludge will be transported to the Fauquier County Water and Sanitation Authority Remington Regional Wastewater Treatment Facility for ultimate processing and disposal.

Once the new treatment works is operational the existing lagoon will be abandoned. The remaining liquid in the pond will be pumped to the new wastewater treatment facility for treatment. Once the pond is dewatered the residual sludge will be lime stabilized and all structures and equipment disinfected and removed. Once sludge stabilization is complete, the pond will be filled in compacted lifts with clean soil, covered with a clay cap and topsoil, and seeded.

RELIABILITY MEASURES.

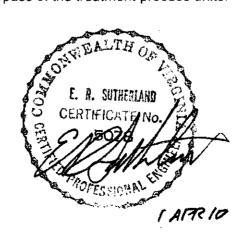
The VPDES Permit designates the facility as Class II Reliability.

Reliability requirements will be attained by the following measures:

All critical facility components (i. e.; equalization pumps, aeration blowers) will have in place, redundant units.

The influent flow equalization basin will have an audible and visible high water alarm.

The facility has the capacity to store between 6,000 gallons and 10,000 gallons on an emergency basis without overflow or bypass of the treatment process units.



Memorandum

Subject: Fauquier Springs Country Club Wastewater Treatment Plant Site Inspection

Date: January 14, 2014

TO: File

From: Joan C. Crowther

On December 16, 2013, I met with Ed Evers, Fauquier Springs Country Club, to inspect the 0.01 MGD wastewater treatment plant. The plant consists of a septic tank followed by an equalization tank, extended aeration plant with UV disinfection and post step aeration. This plant was installed in October 2011 to replace a lagoon. The lagoon has since been properly abandoned and groundwater monitoring is still being conducted to determine the effects of the lagoon while it was in operation.

Fauquier Springs' staff is responsible for performing the maintenance, operation, and monitoring of the wastewater treatment plant. They perform the operational and effluent testing for five days and Environmental System Services (ESS) perform the testing and effluent testing the remaining two days of the week. ESS is under contract to assist should any operational problems occur. ESS also performs the laboratory analysis for the effluent parameters.

The wastewater treatment plant appeared to be operating properly although occasionally molasses has to be fed at the head of the extended aeration plant to keep the "bugs" happy. At the time of the visit, the laboratory records were reviewed and no problems were found as to recording who, when, and what was done at the plant. A detailed laboratory inspection was not performed.

The abandoned lagoon is approximately 150 feet from the shore of the Rappahannock River. A golf fairway is between the lagoon and the Rappahannock River. There is also a drainage swale that runs beside the plant and lagoon across the fairway and enters the Rappahannock River just above the plant's discharge pipe.

The last technical and laboratory inspection for this facility was conducted on December 16, 2004 when the lagoon was still in operation.

To:

Joan C. Crowther

From:

Jennifer Carlson

Date:

August 6, 2013

Subject:

Planning Statement for Fauquier Springs Country Club WWTP

Permit Number:

VA0077411

Information for Outfall 001:

Discharge Type: Municipal

Discharge Flow: 0.02 MGD with a tier for 0.010 MGD

Receiving Stream: Rappahannock River Latitude / Longitude: 38°39'16" / 77°52'32"

Rivermile: 158.41 Streamcode: 3-RPP Waterbody: VAN-E02R

Water Quality Standards: Section 3, Class III, Special Standards - none

Drainage Area: 205.7 Sq.Mil; Topo Map - Jeffersonton, 196B

1. Please provide water quality monitoring information for the receiving stream segment. If there is not monitoring information for the receiving stream segment, please provide information on the nearest downstream monitoring station, including how far downstream the monitoring station is from the outfall.

Outfall 001 discharges to a segment of the Rappahannock River that has not been monitored or assessed. The nearest downstream DEQ ambient water quality monitoring station on the Rappahannock River is located approximately 7.8 miles downstream of Outfall 001. This monitoring station, 3-RPP150.32, is located at the Route 621 bridge crossing. The following is the water quality summary for this segment of the Rappahannock River, as taken from the Draft 2012 Integrated Report*:

Class III, Section 3.

The following are the DEQ monitoring stations located on the Rappahannock River:

- 3-RPP150.32, at Route 621 (ambient water quality)
- 3-RPP150.20, downstream of Route 621 (freshwater probabilistic)

DEQ benthic macroinvertebrate biological monitoring and associated chemical data finds this segment to be fully supporting the aquatic life and wildlife uses. The fish consumption use is fully supporting based on water column metals data.

E. coli monitoring find a bacterial impairment, resulting in an impaired classification for the recreation use. This impairment is nested within the downstream completed bacteria TMDL for the Rappahannock River.

^{*}Virginia's Draft 2012 Integrated Report (IR) has been through the public comment period and reviewed by EPA. The 2012 IR is currently awaiting final approval.

2. Does this facility discharge to a stream segment on the 303(d) list? If yes, please fill out Table A.

No.

3. Are there any downstream 303(d) listed impairments that are relevant to this discharge? If yes, please fill out Table B.

Yes.

Table B. Information on Downstream 303(d) Impairments and TMDLs

Waterbody Name	Impaired Use	Jse Cause on in the Draft 2012 Int		TMDL completed	WLA	Basis for WLA	TMDL Schedule
impaninent mjo	The control of the	Drujt 2012 III	egrated ne	POIL			
						126	
	Recreation	E. coli		Rappahannock	2.405.40	cfu/100ml	
Rappahannock			3.8 miles	River Basin	3.48E+10	E. coli	
River				Bacteria	cfu/year		
				01/23/2008	E. coli	0.02	
						MGD	

^{*}Virginia's Draft 2012 Integrated Report (IR) has been through the public comment period and reviewed by EPA. The 2012 IR is currently awaiting final approval.

4. Is there monitoring or other conditions that Planning/Assessment needs in the permit?

The tidal Rappahannock River, which is located approximately 46 miles downstream of this facility, is listed with a PCB impairment. In support for the PCB TMDL that is scheduled for development by 2016 for the tidal Rappahannock River, this facility is a candidate for low-level PCB monitoring, based upon its designation as a minor municipal facility. Low-level PCB analysis uses EPA Method 1668, which is capable of detecting low-level concentrations for all 209 PCB congeners. DEQ staff has concluded that low-level PCB monitoring is not warranted for this facility, as there are not any stream segments immediately downstream of the facility that are listed with a PCB impairment. Fish tissue monitoring has been conducted on the free flowing Rappahannock River and there have been no exceedances of the fish tissue criterion for PCBs. Based upon this information, this facility will not be requested to monitor for low-level PCBs.

There is a completed downstream TMDL for the aquatic life use impairment for the Chesapeake Bay. However, the Bay TMDL and the WLAs contained within the TMDL are not addressed in this planning statement.

5. Fact Sheet Requirements – Please provide information regarding any drinking water intakes located within a 5 mile radius of the discharge point.

There are no public water supply intakes located within 5 miles of this discharge.

FRESHWATER WATER QUALITY CRITERIA / WASTELOAD ALLOCATION ANALYSIS

Facility Name:

Fauquier Springs

Permit No.: VA0077411

Receiving Stream:

Rappahannock River

Version: OWP Guidance Memo 00-2011 (8/24/00)

Stream Information		Stream Flows		Mixing Information		Effluent Information	
Mean Hardness (as CaCO3) ≃	44.2 mg/L	1Q10 (Annual) ≃	1.42 MGD	Annual - 1Q10 Mix =	4.55 %	Mean Hardness (as CaCO3) =	50 mg/L
90% Temperature (Annual) =	23.4 deg C	7Q10 (Annual) =	1.68 MGD	- 7Q10 Mix =	100 %	90% Temp (Annual) =	26.9 deg C
90% Temperature (Wet season) =	14.8 deg C	30Q10 (Annual) =	3.6 MGD	- 30Q10 Mix =	100 %	90% Temp (Wet season) =	deg C
90% Maximum pH =	7 SU	1Q10 (Wet season) =	16.8 MGD	Wet Season - 1Q10 Mix =	41.84 %	90% Maximum pH =	8.3 \$U
10% Maximum pH =	6.2 \$U	30Q10 (Wet season)	30.4 MGD	- 30Q10 Mix =	100 %	10% Maximum pH =	7.3 SU
Tier Designation (1 or 2) =	2	30Q5 =	6.5 MGD			Discharge Flow =	0.02 MGD
Public Water Supply (PWS) Y/N? =	n	Harmonic Mean ≃	25.2 MGD				
Trout Present Y/N? =	n						
Early Life Stages Present Y/N? =	y						

Parameter	Background		Water Qua	lity Criteria		,	Wasteload	I Allocations			Antidegrada	ition Baselini	3	A	ntidegredatio	n Allocations	i	Most Limiting Allocations			
(ug/l unless noted)	Conc.	Acute	Chronic	HH (PWS)	нн	Acute	Chronic :	HH (PWS)	НН	Acute	Chronic	HH (PWS)	НН	Acute	Chronic	HH (PWS)	нн	Acute	Chronic	HH (PWS)	нн
Acenepthene	0	-	_	· na	9.9E+02		_	па	3.2E+05	-		na	9.9E+01	-		na	3.2E+04			па	3.2E+04
Acrolein	0	_		na	9.3E+00	_		na	3.0E+03	-	_	na	9.3E-01		_	na	3.0E+02			กล	3.0E+02
Acrylonitrile ^C	0	-		na	2.5E+00	-	_	na	3.2E+03	-		na	2.5E-01		_	na	3.2E+02	<u> </u>		па	3.2E+02
Aldrin ^c	Ð	3.0E+00		па	5.0E-04	1.3E+01	_	na	6.3E-01	7.5E-01	_	na	5.0E-05	5.4E+01	_	na	6.3E-02	1.3E+01		na	6.3E-02
Ammonia-N (mg/l)																					
(Yearly) Ammonia-N (mg/l)	0	3.25E+01	3.33E+00	na	-	1.38E+02	6.02E+02	na	**	8.98E+00	8.32E-01	na		6.46E+02	1.51E+02	na		1.38E+02	1.51E+02	па	
(High Flow)	Đ -	3.61E+01	5.81E+00	na	-	1.27E+04	8.83E+03	na		9.02E+00	1.45E+00	na		7.59E+03	2.21E+03	na		7.59E+03	2.21E+03	na	
Anthracene	0	-	_	na	4.0E+04	-		na	1.3E+07		-	na	4.0E+03	-		na	1.3E+06			na	1.3E+06
Antimony	0		_	na	6.4E+02	_	_	na	2.1E+05			na	6.4E+01	-	_	Λà	2.1E+04	_	**	па	2.1E+04
Arsenic	0	3.4E+02	1.5E+02	na	_	1.4E+03	1.3E+04	na		8.5E+01	3.8E+01	na	-	6.1E+03	3.2E+03	na	_	1.4E+03	3.2E+03	na	
Barium	0		_	na				па		-		na				na				na	
Benzene ^C	0	-		пa	5.1E+02		_	na	6.4E+05	-		na	5.1E+01	-		na	6.4E+04			па	6.4E+04
Benzidine ^C	0		•	лa	2.0E-03	_	_	na	2.5E+00			na	2.0E-04	_		na	2.5E-01			na	2.5E-01
Benzo (a) anthracene ^c	0	_	_	na	1.8E-01	_		na	2.3E+02	_	••	na	1.8E-02	_	_	ne	2.3E+01			na	2.3E+01
Benzo (b) fluoranthene ^c	٥		_	na	1.8E-01	_		na	2.3E+02			na	1.8E-02	=	_	na	2.3E+01		••	па	2.3E+01
Benzo (k) fluoranthene ^c	0	-	_	na	1.8E-01		_	na	2.3E+02			na	1.8E-02		_	na	2.3E+01			na	2.3E+01
Benzo (a) pyrene ^c	0	_	-	na	1.8E-01		_	na	2.3E+02			na	1.8E-02		_	na	2.3E+01			na	2.3E+01
Bis2-Chloroethyl Ether ^C	0			na	5.3E+00	-	••	na	6.7E+03		_	na	5.3E-01	_	_	na	6.7E+02			па	6.7E+02
Bis2-Chloroisopropyl Ether	0			na	6.5E+04			na	2.1E+07			na	6.5E+03	_		na	2.1E+06			na	2.1E+06
Bis 2-Ethylhexyl Phthalate c	0	_	-	na	2.2E+01			na	2.8E+04		_	na	2.2E+00		_	na	2.8E+03			na	2.8E+03
Bromoform ^c	0	_		na	1.4E+03	_		па	1.8E+06	_	**	na	1.4E+02	_		na	1.8E+05			na	1.8E+05
Butylbenzylphthalate	0 :			na	1.9E+03			ла	6.2E+05			na	1.9E+02	_	-	ла	6.2E+04			na	6.2E+04
Cadmium	o	1.6E+00	6.0E-01	па	_	6.8E+00	5.1E+01	na	_	3.9E-01	1.5E-01	па	_	2.8E+01	1.3E+01	na	0.22.04	6.8E+00	1.3E+01	па	
Carbon Tetrachloride ^c	0	-		na	1.6E+01	_		na	2.0E+04			na	1.6E+00			na	2.0E+03	3,02.00		na na	2.0E+03
Chlordane ^C	0	2.4E+00	4.3E-03	na	8.1E-03	1.0E+01	3.7E-01	na	1.0E+01	6.0E-01	1.1E-03	na	8.1E-04	4.3E+01	9.1E-02	na	1.0E+00	1.0E+01	9.1E-02	na	1.0E+00
Chloride	0	8.6E+05	2.3E+05	na		3.6E+06	2.0E+07	na		2.2E+05	5.8E+04	na	0.15-04	1.5E+07	4.9E+06	na	1.05+00	3.6E+06	4.9E+06	na	1.02700
TRC	0	1.9E+01	1.1E+01	na		8.0E+01	9.4E+02	na		4.8E+00	2.8E+00	na		3.4E+02	2.3E+02	na		8.0E+01	2.3E+02		
Chlorobenzene	ا ه	1.02.01		na	1.6E+03			na	5.2E+05	4.02.700	2.01.00	na	1.6E+02		-				2.35402	na	5.25+04
31101000112010		_		HQ	1,04,703			i id	U.ZE+03			114	.0E+02	-		na	5.2E+04		-	па	5.2E+04

Parameter	Background		Water Qual	ity Criteria			Wasteload	Allocations			Antidegradat	tion Baseline	9	A	ntidegradatio	on Allocations	- 	l	Most Limitir	ng Allocation	s
(ug/l unless noted)	Conc.	Acute	Chronic	HH (PWS)	HH	Acute	Chronic	HH (PWS)	НН	Acute	Chronic	HH (PWS)	нн	Acute	Chronic	HH (PWS)	нн	Acute	Chronic	HH (PWS)	нн
Chlorodibromomethane ^C	0	_	'	ne	1.3E+02			na	1.6E+05			na	1.3E+01			па	1.6E+04		Cinonic		1.6E+04
Chloraform	0			na	1.1€+04		_	na	3.6E+06	_		па	1.1E+03		-	กล	3.6E+05		-	па	1.6E+04 3.6E+05
2-Chloronaphthalene	٥			na	1.6E+03	-	_	na	5.2E+05		-	na	1.6E+02	-		na	5.2E+04		_	na	5.2E+04
2-Chlorophenol	٥		-	na	1.5E+02	_	_	na	4.9E+04			na	1.5E+01	_				1		na	
Chlorpyrifos	0	8.3E-02	4.1E-02	na		3.5€-01	3.5E+00	ла	4.50.704	2.1E-02	1.0E-02		1.SE-F01	1 55.00	0.75.04	na	4.9E+03			na	4.9E+03
Chromium III	0	3.0E+02	3.8E+01	na	-	1.3E+03	3.2E+03	na	_	7.3E+01	9.5E+00	na		1.5E+00	8.7E-01	na	-	3.5E-01	8.7E-01	na	
Chromium VI	o	1.6E+01	1.1E+01	na	_	6.8E+01	9.4E+02	na	_	4.0E+00	2.8E+00	па	-	5.3E+03	8.1E+02	na 	-	1.3E+03	8.1E+02	па	-
Chromium, Total	0	1.02.01	1.12.401	1.0E+02	-	0.02.701	5.4E+02			4.06+00		na 4 DE : D4	-	2.9E+02	2.3E+02	na	-	8.8E+01	2.3E+02	na	•-
Chrysene C	ŏ		_		1.8E-02		-	na	2.25.04	_		1.0E+01			-	3,3E+03				na	-
₋ '	a	6.4E+00	4.5E+00	na		0.75.04	0.05.00	na	2.3E+01	-	-	na	1.8⊱-03	-	-	na	2.3E+0D		**	na	2.3E+00
Copper .	0			na	4.05.04	2.7E+01	3.8E+02	па		1.6E+00	1.1E+00	na	-	1.1E+02	9.5E+01	na	-	2.7E+01	9.5E+01	na	
Cyanide, Free	a	2.2E+01	5.2E+00	na	1.6E+04	9.3E+01	4.4E+02	na	5.2E+06	5.5E+00	1.3E+00	na	1.6E+03	4.0E+02	1.1E+02	na	5.2E+05	9.3E+01	1.1E+02	nа	5.2E+05
DDE.c	-	-		na	3.1E-03	_	-	กล	3.9E+00	~		na	3.1E-04	-	-	na	3.9E-01	••		na	3.9E-01
DDT °	0			na	2.2E-03		-	na	2.8E+00		_	па	2.2E-04	-	-	ла	2.8E-01			na	2.8E-01
1	0	1.1E+00	1.0E-03	na	2.2E-03	4.7E+00	8.5E-02	กล	2.8E+00	2.8E-01	2.5E-04	na	2.2E-04	2.0E+01	2.1E-02	па	2.8E-01	4.7E+00	2.1E-02	na	2.8E-01
Demeton	0	_	1.0E-01	na	-	-	8.5E+00	na	-	-	2.5E-02	na	-	-	2.1E+00	na			2.1E+00	na	
Diazinon	0	1.7E-01	1.7E-01	กล		7.2E-01	1.4E+01	ná	-	4.3E-02	4.3E-02	na	-	3.1E+00	3.6E+00	na	-	7.2E-01	3.6E+00	na	-
Dibenz(a,h)anthracene ^c	0	-	-	na	1.8E-01	-		na	2.3E+02	-	~	па	1.8E-02	_	-	na	2.3E+01	-		na	2.3E+01
1,2-Dichlorobenzene	0	-		na	1.3E+03	-		na	4.2E+05			па	1.3E+02	-		na	4.2E+04			na	4.2E+04
1,3-Dichlorobenzene	0	-	*-	na	9.6E+02	-	-	na	3.1E+05	-	-	па	9.6E÷01	~		na	3.1E+04	-		па	3.1E+04
1,4-Dichlorobenzene	0	-	-	na	1.9E+02	-	-	ne	6.2E+04	-	-	na	1.9E+01	-	-	na	6.2E+03			na	6.2E+03
3,3-Dichlorobenzidine ^C	0	-		na	2.8E-01	-	-	na	3.5E+02	-		na	2.8E-02	•-		na	3.5E+01			na	3.5E+01
Dichlorobromomethane ^c	0	_	-	па	1.7E+02	-	-	na	2.1E+05	-		na	1.7E+01	_	_	ла	2.1E+04	-		na	2.1E+04
1,2-Dichloroethane ^c	0	~	-	na	3.7E+02	-	-	na	4.7E+05			na	3.7E+01			na	4.7E+04			na	4.7E+04
1,1-Dichloroethylene	0	-	-	na	7.1E+03	-	-	na	2.3E+06		-	na	7.1E+02			na	2.3E+05			na	2.3E+05
1,2-trans-dichloroethylene	0	-		กล	1.0E+04	-	-	na	3.3E+06			na	1.0E+03	-		na	3.3E+05			na	3.3E+05
2,4-Dichlorophenol	0			na	2.9E+02		~	na	9.5E+04			na	2.9E+01		_	na	9.5E+03		••	na	9.5E+03
2,4-Dichlorophenoxy acetic acid (2,4-D)	0 1			na	_			na					Ī								
1,2-Dichloropropane ^C	0	_	_	na	1.5E+02	_	_		105,05	_	-	na	4.55.04	_	-	na	-	-		na	-
1,3-Dichloropropene ^C	Ö	-	_	na	2.1E+02	-	-	па	1.9E+05	_	_	na	1.5E+01			na	1.9E+04			na	1.9E+04
Dieldrin C	0	2.45.01	5.6E-02			4.05 (00	4.05.00	na 	2.6E+05	-	4.45.00	na	2.1E+01			na	2.6E+04			na	2.6E+04
ļ .	l	2.4E-01	3.0E-02	na	5.4E-04	1.0E+00	4.8E+00	ла	6.8E-01	6.0E-02	1.4E-02	па	5.4E-05	4.3E+00	1.2E+00	na	6.8E-02	1.0E+00	1.2E+00	na	6.8E-02
Diethyl Phthalate	0		-	na	4.4E+04	,		กล	1.4E+07		-	na	4.4E+03	_		na	1.4E+06	-	-	na	1.4E+06
2,4-Dimethylphenol	0			na 	8.5E+02	_	-	na	2.8E+05	-	-	na	6.5E+01	_	-	na	2.8E+04		-	na	2.8E+04
Dimethyl Phthalate	0	-	-	na	1.1E+06	-	_	na	3.6E+08		-	na	1.1E+05	-	~	na	3.6E+07	-		па	3.6E+07
Di-n-Butyl Phthalate	0	-	_	na	4.5E+03	-		na	1.5E+06		-	na	4.5E+02	-	-	na	1.5E+05			na	1.5E+05
2,4 Dinitrophenol	0	~		na	5.3E+03			па	1.7E+06	-		na	5.3E+02	-		na	1.7E+05	••		па	1.7E+05
2-Methyl-4,6-Dinitrophenol	0		-	na	2.8E+02			na	9.1E+04	-		na	2.8E+91	~-		na	9.1E+03			na	9.1E+03
2,4-Dinitrototuene ^c Dioxin 2,3,7,8- tetrachlorodibenzo-p-dioxin	0	-	-	na	3.4E+01	-	~	na	4.3E+04		-	na	3.4E+00	-	-	na	4.3E+03		-	na	4.3E+03
·	· ·		wh	na	5.1E-08		-	na	1.7E-05	_		na	5.1E-09		-	na	1.7E-06			na	1.7E-06
1,2-Diphenylhydrazine ^c	0			па	2.0E+00	_	-	па	2.5E+03	-	=	กล	2,0E-01		-	па	2.5E+02	**		na	2.5E+02
Alpha-Endosulfan	0	2.2E-01	5.6E-02	na	8.9E+01	9.3E-01	4.8E+00	na	2.9E+04	5.5E-02	1.4E-02	na	8.9E+00	4 0E+00	1.2E+00	па	2.9E+03	9.3E-01	1.2E+00	na	2.9E+03
Beta-Endosulfan	0	2.2E-01	5.6E-02	na	8.9E+01	9.3E-01	4.8E+00	na	2.9E+04	5.5E-02	1.4E-02	па	8.9E+00	4.0E+00	1.2E+00	na	2.9E+03	9.3E-01	1.2E+00	na	2.9E+03
Alpha + Beta Endosulfan	G	2.2E-01	5.6E-02	~	-	9.3E-01	4.8E+00	-	~	5.5E-02	1.4E-02	-	-	4.0E+00	1.2E+00	-		9.3E-01	1.2E+00		
Endosulfan Sulfate	0	-	-	na	8.9E+01		-	na	2.9E+04	-		na	8.9E+00	-	-	na	2.9E+03	-		na	2.9E+03
Endrin	0	8.6E-02	3.6E-02	na	6.0E-02	3.6E-01	3.1E+00	na	2.0E+01	2.2E-02	9.0E-03	na	6.0E-03	1.5€+00	7.7E-01	na	2.0E+00	3.6E-01	7.7E-01	na	2.0E+00
Endrin Aldehyde	. 0			na	3.0E-01	-		na	9.8E+01			na	3.0E-02	-		na	9.8E+00			па	9.8E+00

Parameter	Background		Water Qual	ity Criteria		_	Wasteload	Allocations			Antidegradat	ion Baselin	e	А	ntidegradati	on Allocation	s		Most Limiti	ng Allocations	
(ug/l unless noted)	Conc.	Açule	Chronic	HH (PWS)	HH	Acute	Chronic	HH (PWS)	нн	Acute	Chronic	HH (PWS)	нн	Acute	Chronic	HH (PWS)	НН	Acute	Chronic	HH (PWS)	нн
Ethylbenzene	0			na	2.1E+03	-		na	6.8E+05			na	2.1E+02		-	na	6.8E+04			na	6.BE+04
Fluoranthene	0			na	1.4E+02			na	4.6E+04			na	1.4E+01		_	na	4.6E+03	-		na	4.6E+03
Fluorene	0		-	na	5.3E+03	_	_	กล	1.7E+06		→	na	5.3E+02		_	na	1.7E+05			na	1.7E+05
Foaming Agents	0		_	na	-	-	*-	na		_		na	**	_		us.			- -	na	••
Guthion			1.0E-02	na	_		8.5E-01	na			2.5E-03	na	_		2.1E-01	กล		_	2.1E-01	na	••
Heptachlor ^C	o	5.2E-01	3.8E-03	na	7.9E-04	2.2E+00	3.2E-01	na	1.0E+00	1.3E-01	9.5E-04	na	7.9€-05	9.4E+00	8.1E-02	na	1.0E-01	2.2E+00	8.1E-02	na	1.0E-01
Heptachlor Epoxide ^C	0	5.2E-01	3.8E-03	na	3.9E-04	2.2E+00	3.2E-01	na	4.9E-01	1.3E-01	9.5E-04	na	3.9E-05	9.4E+00	8.1E-02	na	4.9E-02	2.2E+00	8.1E-02	па	4.9E-02
Hexachlorobenzene ^C	0	J.ZL-01	0.0L-00	na	2.9E-03	2.20.00		na	3.7E+00	1.02-01	3.52-04	na	2.9E-04	3.41.700	D. 1L-02	na.	3.7E-01				3.7E-01
Hexachlorobutadiene ^C	0	-		na	1.8E+02	_	_	na	2.3E+05			na	1.8E+01	_	-	na	2.3E+04	••		na	2.3E+04
Hexachlorocyclohexane	Ĭ			ri q	1.01. 102	_		110	2.50,00]	_	11a),OL-101		_	iia.	2.36104			na	2,35404
Alpha-BHC ^c	0	_		na	4.9E-02	-		na	6.2E+01	_	_	กล	4.9E-03		_	na	6.2E+00			na	6.2E+00
Hexachlorocyclohexane	-																				
Beta-BHC ^C	0		-	na	1.7E-01	-	-	na	2.1E+02	-	-	na	1.7E-02		-	na	2.1E+01	••		na	2.1E+01
Hexachtorocyclohexane					4.05.00	4.05.00															
Gamma-BHC ^c (Lindane)	0	9.5E-01	na	na	1.8E+00	4.0E+00	-	na	2.3E+03	2.4E-01		กล	1.8E-01	1.7E+01	••	na	2.3E+02	4.0E+00		na	2.3E+02
Hexachlorocyclopentadiene	0	_	-	na	1.1E+03	-	-	na	3.6E+05	~	-	na	1.1E+02	_		na	3.6E+04		-	na	3.6E+04
Hexachioroethane ^C	0		-	na	3.3E+01	-	••	na	4.2E+04		-	na	3.3E+00	-		na	4.2E+03	••	••	na	4.2E+03
Hydrogen Sulfide	0	-	2.0E+00	na	_		1.7E+02	na	-		5.0E-01	na	 -	-	4.3E+01	ла	-		4.3E+01	na	
Indeno (1,2,3-cd) pyrene ^C	0	-	-	na	1.8E-01	-		na	2.3E+02		_	na	1.8E-02	-	-	na	2.3E+01		-	na	2.3E+01
Iron	0	_	-	na				na	-		-	na			-	na			-	na	
Isophorone ^C	0		-	ла	9.6E+03	-	_	na	1.2E+07	-		na	9.6E+02	-	-	na	1.2E+06			па	1.2E+06
Kepone	0	-	0.0E+00	ña			0.0E+00	na			0.0E+00	na	-	-	0.0E+00	na	-	_	0.016+00	na	
Lead	0	4.4E+01	4.8E+00	na	-	1.8E+02	4.1E+02	na	- !	1.1E+01	1.2E+00	na	-	7.6E+02	1.0E+02	na	-	1.8E+02	1.0E+02	na	**
Malathion	0	-	1.0E-01	na	**	~	8.5E+00	na	-		2.5E-02	na		-	2.1E+00	na	-		2.1E+00	na	
Manganese	٥			na	-	-		na			-	па		-	-	na	••		-	na	
Mercury	0	1.4E+00	7.7E-01			5.9E+00	6.5E+01			3.5E-01	1.9E-01		-	2.5 E+0 1	1.6E+01	••	-	5.9E+00	1.6E+01		••
Methyl Bromide	0	-	-	na	1.5E+03	-	**	na	4.9E+05		-	na	1.5E+02			na	4.9E+04	••		na	4.9E+04
Methylene Chloride ^C	0		-	na	5.9E+03	-		na	7.4E+06	_	-	na	5.9E+02			na	7.4E+05	•••		na	7.4E+05
Methoxychlor	0	_	3.0E-02	na	-	-	2.6E+00	na	-		7.5E-03	пa	-		6.4E-01	na			6.4E-01	na	
Mirex	0	-	0.0E+00	na		-	0.0E+00	na		-	0.0E+00	na			0.0E+00	na	-		0.0E+00	na	
Nickel	0	9.4E+01	1.0E+01	na	4.6E+03	4.0E+02	8.6E+02	na	1.5E+06	2.3E+01	2.5E+00	na	4.6 £ +02	1.6E+03	2.2E+02	na	1.5E+05	4.0E+02	2.2E+02	па	1.5E+05
Nitrate (as N)	0	-	_	na	-	-		na	-		-	na	-	·		na		_	••	na	
Nitrobenzene	٥	_	-	na	6.9E+02	-		na	2.2E+05	_		па	6.9E+01	_	••	na	2.2E+04	_	••	па	2.2E+04
N-Nitrosodimethylamine ^C	0	_		na	3.0E+01		**	na	3.8E+04			na	3.0€+00		_	па	3.8E+03		_	па	3.8E+03
N-Nitrosodiphenylamine ^C	0		-	na	6.0E+01		_	na	7.6E+04	_		па	6.0E+00		_	na	7.6E+03			na	7.6E+03
N-Nitrosodi-n-propylamine ^C	o			na	5.1E+00		_	па	6.4E+03			па	5.1E-01			na	6.4E+02			na	6.4E+02
Nonylphenol	0	2.8E+01	6.6E+00		_	1.2E+02	5.6E+02	na		7,0E+00	1.7E+00		_	5.0E+02	1.4E+02	_	_	1,2E+02	1.4E+02	па	
Parathion	o	6.5E-02	1.3E-02	na		2.7E-01	1.1E+00	na	-	1.6E-02	3.3E-03	na	{	1.2E+00	2.8E-01	na		2.7E-01	2.8E-01	na	
PCB Total ^C	o l		1.4E-02	na	6.4E-04	-	1.2E+00	na	8.1E-01		3.5E-03	na	6.4E-05	_	3.0E-01	na	8.1E-02		3.0E-01	na	8.1 <u>E</u> -02
Pentachlorophenol ^C	0	4.3E+00	3.0E+00	na	3.0E+01	1.8E+01	2.6E+02	na	3.8E+04	9.8E-01	7.5E-01	na	3.0E+00	7.1E+01	6.4E+01	na	3.8E+03	1.8E+01	6.4E+01	na	3.8E+03
Phenol	0	_	_	na	8.6E+05		_	па	2.8E+08			na	8.6E+04			na.	2.8E+07		0.42701	na	2.8E+07
Pyrene	0			na	4.0E+03	_	_	na	1,3E+06			na	4.0E+02		_	na	1.3E+05		- -		1.3E+05
Radionuclides	o			na		_		na					4.02+02		_		1.30705			na	
Gross Alpha Activity		_	-	140	_		_	i i di	-			na	-	_		na	~	**	••	na	••
(pCi/L)	٥		-	na	-	-		กล		·		na	-		-	na	- 1	••		na	
Beta and Photon Activity (mrem/yr)	0			na	_	_		лa	_	_	_	na	~	_	_	00				пэ	
Radium 226 + 228 (pCi/L)	o	_	•-	กล	-	-		na		_	_	na			-	na	_ [па	_
Uranium (ug/l)	0	_					-			_	-					na	- 1		••	na	
Cresium (ugn)				na		-	~-	กล				na				na				na	

Parameter	Background		Water Qua	lity Criteria	<u> </u>		Wasteload	Allocations			Antidegradat	tion Baseline	9		ntidegradatio	n Allocations		T	Moet Limiti	ng Allocations	
(ug/l unless noted)	Conc.	Acute	Chronic	HH (PWS)	НН	Acute	Chronic	HH (PWS)	HH	Acute	· ·	HH (PWS)		Acute	7	HH (PWS)	HH	Acute	Chronic	HH (PWS)	HH
Selenium, Total Recoverable	0	2.0E+01	5.0E+00	na	4.2E+03	8.5E+01	4.3E+02	na	1.4E+06	5.0E+00	1.3E+00	na na	4.2E+02	3.6E+02	1.1E+02	na	1.4E+05	8.5E+01	1.1E+02	na (FVS)	1.4E+05
Silver	0	8.9E-01	_	na	_	3.8E+00		na	_	2.1E-01		na	_	1.5E+01	-	na	-	3.8E+00		na	
Sulfate	0		_	na	***			na				na			_	na	-	0.02.00	-		~
1,1,2,2-Tetrachloroethane ^C	0			na	4.0E+01	-	_	na	5.0E+04	<u> </u>	_	na	4.0E+00		_	na	5.0E+03			na	-
Tetrachloroethylene ^C	О	-		na	3.3E+01	_		na	4.2E+04	_	_	na	3.3E+00		_	na	4.2E+03	_		na	5.0E+03
Thallium	0	_		na	4.7E-01	_		па	1.5E+02			na	4.7E-02		-		1.5E+01	••		na	4.2E+03
Toluene	0		_	na	6.0E+03		_	па	2.0E+06		_	na	6.0E+02			na		••	-	na	1.5E+01
Total dissolved solids	0			na		_		na	2.02.00	"	-			-		na	2.0E+05		-	na	2.0E+05
Toxaphene ^c	0	7.3E-01	2.0E-04	na	2.8E-03	3.1E+00	1.7E-02	na	3.5E+00	4.05.04	- AF	na		105.01	-	na				na	-
Tributykin	o	4.6E-01	7.2E-02							1.8E-01	5.0E-05	na	2.8E-04	1.3E+01	4.3E-03	na	3.5E-01	3.1E+00	4.3E-03	กล	3.5E-01
1,2,4-Trichlorobenzene	ŏ	4.02-01		na	7.05.04	1.9E+00	6.1E+00	na		1.2E-01	1.8E-02	na		8.3E+00	1.5E+00	na	-	1.9E+00	1.5E+00	na	
1,1,2-Trichloroethane ^C	ا د	-	-	na	7.0E+01			na	2.3E+04	-		na	7.0E+00			na	2.3E+03		-	na	2.3E+03
	١ ،	-		na	1.6E+02	-	-	na	2.0E+05			na	1.6E+01	-	-	па	2.0E+04			na	2.0E+04
Trichloroethylene ^C	· ·		***	na	3.0E+02		-	na	3.8E+05		_	па	3.0E+01			na	3.8E+04	**	-	na	3.8E+04
2,4,6-Trichlorophenol C	0		-	na	2.4E+01	-	-	na	3.0E+04		-	na	2.4E+00		-	na	3.0E+03		-	na	3.0E+03
2-(2,4,5-Trichlorophenoxy) propionic acid (Silvex)	0	_		na	-			na				na		_	_	na	**			na	
Vinyl Chloride ^C	0			กล	2.4E+01	-	-	na	3.0E+04			na	2.4E+00	_	_	na	3.0E+03			na	3.0E+03
Zinc	0	6.0E+01	5.9E+01	na	2.6E+04	2.5E+02	5.0E+03	กล	8.5E+06	1.5E+01	1.5E+01	па	2.6E+03	1.1E+03	1.3E+03	na	8.5E+05	2.5E+02	1.3E+03	na	8.5E+05

Notes:

- 1. All concentrations expressed as micrograms/liter (ug/l), unless noted otherwise
- 2. Discharge flow is highest monthly average or. Form 2C maximum for Industries and design flow for Municipals
- 3. Metals measured as Dissolved, unless specified otherwise
- 4. "C" indicates a carcinogenic parameter
- Regular WLAs are mass balances (minus background concentration) using the % of stream flow entered above under Mixing Information. Antidegradation WLAs are based upon a complete mix.
- 6. Antideg. Baseline = (0.25(WQC background conc.) + background conc.) for acute and chronic
 - = (0.1(WQC background conc.) + background conc.) for human health
- 7. WLAs established at the following stream flows: 1Q10 for Acute, 30Q10 for Chronic Ammonia, 7Q10 for Other Chronic, 30Q5 for Non-carcinogens and Harmonic Mean for Carcinogens. To apply mixing ratios from a model set the stream flow equal to (mixing ratio 1), effluent flow equal to 1 and 100% mix.

Metal	Target Value (SSTV)
Antimony	2.1E+04
Arsenic	5.8E+02
Barium	na
Cadmium	2.7E+00
Chromium III	4.8E+02
Chromium VI	2.7E+01
Copper	1.1E+01
Iron	na
Lead	6,1E+01
Manganese	na
Mercury	2.4E+00
Nickel	1.3E+02
Selenium	3,4E+01
Silver	1.5E+00
Zinc	1.0E+02

Note: do not use QL's lower than the minimum QL's provided in agency guidance

0.020 MGD DISCHARG	GE FLOW - STREAM MIX PER "Mix.exe"	
Discharge Flow Used for WQS-WLA Calculations (MGI 0,020	Ammonia - Dry Season - Acute	Ammonia - Dry Season - Chronic
Stream Flows Total Mix Flows Allocated to Mix (MGD) Dry Season Wet Season Dry Season Wet Season Dry Season Wet Season Ones Ones	90th Percentile pH (SU) 7.110 (7.204 - pH) 0.094 (pH - 7.204) -0.094 Trout Present Criterion (mg N/l 32.517 Trout Absent Criterion (mg N/L 32.517 Trout Present? n Effective Criterion (mg N/L) 32.517	90th Percentile Temp. (deg C) 23.419 90th Percentile pH (SU) 7.002 MIN 1.606 MAX 23.419 (7.688 - pH) 0.686 (pH - 7.688) -0.686 Early LS Present Criterion (mg N 3.326 Early LS Absent Criterion (mg N 3.326 Early Life Stages Present? y Effective Criterion (mg N/L) 3.326
Dry Season Wet Season 1Q10 90th% Temp. Mix (deg C) 24,227 14,758	Ammonia - Wet Season - Acute	Ammonia - Wet Season - Chronic
30Q10 90th% Temp. Mix (deg C) 23.419 14.790 1Q10 90th% pH Mix (SU) 7.110 7.001 30Q10 90th% pH Mix (SU) 7.002 7.000 1Q10 10th% pH Mix (SU) 6.307 N/A 7Q10 10th% pH Mix (SU) 6.205 N/A Calculated Formula Inputs 1Q10 Hardness (mg/L as CaCO3) 45.6 45.6 7Q10 Hardness (mg/L as CaCO3) 44.3 44.3	90th Percentile pH (SU) 7.001 (7.204 - pH) 0.203 (pH - 7.204) -0.203 Trout Present Criterion (mg N/L 36.056 Trout Present? n Effective Criterion (mg N/L) 36.056	90th Percentile Temp. (deg C) 90th Percentile pH (SU) 7.000 MIN 2.801 MAX 14.790 (7.688 - pH) 0.688 (pH - 7.688) Early LS Present Criterion (mg N) Early LS Absent Criterion (mg N) Early Life Stages Present? y Effective Criterion (mg N/L) 5.806

			0.020	MGD DISCHAF	RGE FLOW - COMPLETE STREA	M MIX		
Discharge Flo	w Used for W	/OS-WLA Cal	culations (MGI	0.020	Ammonia - Dry Season - Acu	<u>rte</u>	Ammonia - Dry Season - Chro	<u>nic</u>
1Q10 7Q10 30Q10 30Q5 Harm. Mean Annual Avg.	100% Str Allocated to Dry Season 1.420 1.680 3.600 6.500 25.200 0.000	eam Flows o Mix (MGD) Wet Seasor 16.800 N/A 30.400 N/A N/A N/A N/A	Total M <u>Stream + Dis</u> <u>Dry Season</u> 1.440 1.700 3.620 6.520 25.220 0.020	Mix Flows scharge (MGD)	90th Percentile pH (SU) (7.204 - pH) (pH - 7.204) Trout Present Criterion (mg N/I Trout Absent Criterion (mg N/L Trout Present? Effective Criterion (mg N/L)	7.006 0.198 -0.198 23.981 35.910 n 35.910	90th Percentile Temp. (deg C) 90th Percentile pH (SU) MIN MAX (7.688 - pH) (pH - 7.688) Early LS Present Criterion (mg N Early LS Absent Criterion (mg N) Early Life Stages Present? Effective Criterion (mg N/L)	23.419 7.002 1.606 23.419 0.686 -0.686 3.326 3.326 y 3.326
1010 00150/	Temp. Mix (de	· · · · · · · ·	Dry Season 23,449	Wet Season 14.782	Ammonia - Wet Season - Acu	ute	Ammonia - Wet Season - Chro	nic
30Q10 90th% 1Q10 90th% 30Q10 90th% 1Q10 10th% 7Q10 10th%	Temp. Mix (oph Mix (SU) pH Mix (SU) ss (mg/L as C	eg Ć) (aCO3) =	23.419 7.006 7.002 6.206 6.205	14.792 14.790 7.000 7.000 N/A N/A Formula Inputs 44.281 44.268	90th Percentile pH (SU) (7.204 - pH) (pH - 7.204) Trout Present Criterion (mg N/I Trout Absent Criterion (mg N/L Trout Present? Effective Criterion (mg N/L)	7.000 0.204 -0.204 24.093 36.077 n 36.077	90th Percentile Temp. (deg C) 90th Percentile pH (SU) MIN MAX (7.688 - pH) (pH - 7.688) Early LS Present Criterion (mg N Early LS Absent Criterion (mg N Early Life Stages Present? Effective Criterion (mg N/L)	14.790 7.000 2.801 14.790 0.688 -0.688 5.806 5.806 y 5.806

Fauquier Springs Country Club Effluent Data November 2011 through October 2013

Month/			
Year	Day	Temp °C	рН
Nov-11	1	17.6	7.5
	2	16.9	7.5
	3	17.3	7.5
	4	18.3	7.0
	5	16.7	7.5
	6	17.3	7.5
	7	17.0	7.5
	8	17.3	7.5
	9	18.1	7.5
	10	17.1	70
	11	17.3	7.5
	12	16.5	7.5
	13	17.7	7.5
	14	18.5	7.5
	15	18.2	7.5
	16	18.8	7.5
	17	18.3	7.0
	18	17.1	7.5
	19	17.7	7.2
	20	16.7	7.0
	21	17.5	7.5
	22	17.8	7.5
	23	17.8	7.5
	24	17.5	7.5
	25	16.4	7.5
	26	17.4	7.0
	27	18.5	7.0
	28	17.5	7.3
<u> </u>	29	17.4	7.5
	30		7.5
Dec-11	1	17.0	7.5
Dec-11	2	16.5	
		15.7	7.5
	3 4	15.7 15.7	7.5 7.5
-			
	5	17.0	7.5
<u> </u>	- 6	17.1	7.5
<u> </u>	7	17.5	7.5
—	8	17.0	7.5
	9	15.9	7.5
	10	13.7	7.0
	11	13.1	7.5
	12	12.0	7.5
	13	11.2	7.5
	14	10.9	7.3
	15	12.7	7.0

Month/ Year	Day	Temp °C	pН
	16	13.2	7.5
	17	12.1	7.5
	18	12.0	7.0
	19	12.6	7.5
	20	10.5	7.3
	21	11.3	7.5
	22	11.6	7.5
	23	12.0	7.5
	24	11.7	7.5
	25	10.7	7.0
	26	8.9	7.5
	27	8.3	7.5
	28	8.9	7.5
	29	8.7	7.0
	30	9.7	7.0
	31	4.7	7.0
Jan-12	1	3.3	7.5
JUN 12	2	9.9	7.5
	3	8.1	7.0
	4	6.7	7.0
	5	7.0	7.5
	6	7.0	7.3
	7	8.9	7.6
	8	7.5	7.7
	9	10.6	7.7
	10	10.7	7.7
	11	7.9	7.5
	12	9.1	7.3
	13	9.6	7.5
	14	4.7	7.6
	15	4.4	7.5
ļ	16	10.4	7.7
	17	10.2	7.2
	18	10.3	7.6
	19	8.9	7.5
	20	8.6	7.5
	21	7.9	7.4
	22	11.6	7.4
	23	9.1	7.4
	24	11.2	7.3
	25	10.2	7.4
	26	10.1	7.3
	27	12.5	7.4
	28	9.8	7.3
	29	7.1	7.4

Month/			
Year	Day	Temp °C	pН
	30	12.6	7.4
	31	12.4	7.4
Feb-12	1	13.2	7.3
	2	13.4	7.3
	3	13.0	7.4
	4	10.5	7.3
	5	13.3	7.3
	6	12.9	7.3
	7	11.8	7.4
	8	11.6	7.3
	9	10.1	7.4
	10	10.3	7.6
	11	10.7	7.4
	12	5.1	7.3
	13	10.1	7.5
	14	10.4	7.6
	15	11.6	7.4
-	16	12.4	7.4
	17	13.0	7.3
	18	13.4	7.5
	19	13.4	7.5
	20	13.5	7.5
	21	12.9	7.6
	22	12.7	7.6
	23	12.9	7.3
	24	13.8	7.4
	25	12.7	7.3
	26	13.7	7.3
	27	15.4	7.5
	28	15.0	7.5
	29	13.9	7.6
Mar-12	1	14.1	7.5
	2	13.9	7.4
	3	14.2	7.2
	4	14.4	7.1
	5	13.8	7.3
	6	12.1	7.2
	7	12.4	7.5
	8	13.3	7.4
	9	14.8	7.3
	10	7.5	7.3
	11	7.3	7.3
	12	15.0	7.3
	13	15.7	7.2
	14	17.3	7.2

Month/	.	Town %	-11
Year	Day	Temp °C	pH
	15	18.1	7.1
	16	18.6	7.2
	17	20.1	7.1
<u> </u>	18	20.8	7.1
	19	18.4	7.4
	20	19.6	7.3
	21	18.8.	7.3
	22	18.7	7.2
	23	19.5	7.4
	24	14.7	7.2
	25	13.5	7.3
	26	20.1	7.3
	27	18.7	7.3
	28	18.5	7.2
	29	18.4	7.4
	30	18.3	7.3
	31	16.1	7.3
Apr-12	1	16.7	7.2
	2	20.0	7.2
	3	18.6	7.4
	4	18.9	7.3
	5	18.5	7.2
	6	18.3	7.3
	7	16.7	7.5
	8	17.3	7.3
	9	17.8	7.2
	10	18.8	7.4
	11	18.2	7.5
	12	18.1	7.4
	13	18.0	7.5
	14	8.9	7.8
	15	12.6	7.5
	16	19.8	7.2
	17	20.3	7.9
	18	19.4	8.2
	19	19.8	7.7
	20	19.8	8.1
	21	20.4	8.0
	22	18.5	8.5
	23	18.6	8.5
	24	18.8	8.1
	25	18.8	8.0
	26	18.6	8.5
	27	19.4	8.1
	28	10.1	8.0
	29	10.5	7.9
	30	19.8	8.0

Month/			
Year	Day	Temp °C	рН
May-12	1	203	7.4
	2	21.8	8.0
	3	22.1	7.3
	4	22.9	8.1
	5	22.5	7.9
	6	22.6	8.5
	7	22.5	8.3
	8	22.4	8.2
	9	22.8	7.5
	10	22.0	7.7
	11	21.7	8.1
	12	9.5	7.7
	13	16.8	7.7
	14	23.1	8.4
	15	23.3	7.5
	16	23.8	7.6
	17	22.7	8.4
	18	22.1	7.7
	19	20.8	8.5
	20	22.7	8.2
	21	23.4	8.1
	22	23.4	7.8
	23	23.2	7.9
	24	23.1	7.8
	25	23.6	8.3
	26	22.7	7.8
	27	23.2	7.7
	28	24.8	8.1
	29	24.9	7.9
	30	25.1	8.0
	31	25.3	8.0
Jun-12	1	25.1	8.1
	2	21.8	7.5
	3	24.0	7.7
	4	23.5	7.9
	5	18.0	9.3
	6	23.3	8.2
	7	20.9	8.2
	8	23.6	8.2
	9	22.4	8.1
	10	24.8	8.5
	11	25.1	8.2
	12	23.0	8.3
	13	25.5	8.1
	14	24.8	8.4
	15	23.8	7.9
	16	23.5	7.8

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Month/ Year	Day	Temp °C	рН
	17	22.8	8.0
	18	25.0	8.0
	19	25.1	8.0
	20	26.5	8.1
	21	26.3	7.7
	22	26.9	7.8
	23	25.8	8.2
	24	26.6	7.8
	25	26.2	8.0
	26	25.9	7.8
	27	26.0	7.4
	28	25.9	7.9
	29	26.7	8.3
	30		
Jul-12	1	27.8	7.4
	2	25.5	8.2
	3	26.8	8.7
	4	26.1	8.4
	5	27.9	8.6
	6	28.0	8.3
	7	28.1	8.8
	8	29.2	8.7
	9	27.6	8.4
	10	26.8	8.2
	11	26.2	8.1
	12	27.5	8.3
	13	27.3	7.7
	14	27.6	8.3
	15	27.4	8.2
	16	25.7	8.2
	17	28.3	81
	18	27.7	81
	19	28.0	8.1
	20	28.1	8.2
	21	27.2	8.6
	22	27.3	8.6
	23	27.7	8.1
	24	28.2	8.3
	25	27.4	8.4
	26	27.3	7.9
	27	27.7	8.0
	28	27.0	8.4
	29	27.2	8.2
	30	27.5	8.2
	31	27.7	7.0
Aug-12	1	27.6	8.6
	2	27.4	8.4

Month/	<u> </u>	l :		Month/	Ι			N	Month/			<u> </u>
Year	Day	Temp °C	ρН	Year	Day	Temp °C	рН		Year	Day	Temp °C	рН
	3	27.9	8.5		19	25.5	8.1			5	16.7	7.5
	4	27.7	8.3	1	20	24.2	8.1			6	17.3	7.5
	5	27.6	8.3		21	23.5	7.9]		7	17.0	7.5
	6	28.1	8.5		22	25.1	8.0	1		8	17.3	7.5
	7	28.3	8.5		23	24.2	8.2			9	18.1	7.5
	8	28.0	8.2		24	23.7	8.2			10	17.1	7.0
	9	27.8	8.0		25	22.8	8.1			11	17.3	7.5
	10	27.7	8.2		26	23.4	8.0			12	16.5	7.5
	11	27.4	8.0		27	24.0	8.1			13	17.7	7.5
	12	27.3	8.2		28	24.5	8.2			14	18.5	7.5
	13	27.9	8.5		29	24.3	8.2			15	18.2	7.5
	14	27.2	8.4		30	24.0	8.2			16	18.8	7.5
	15	27.4	8.4	Oct-12	1	24.0	8.3			17	18.3	7.0
	16	27.0	8.2		2	23.7	8.2			18	17.1	7.5
	17	27.2	8.2		3	24.2	8.1			19	17.7	7.2
	18	26.9	9.0		4	24.5	7.7			20	16.7	7.0
	19	26.8	8.1		5	22.9	8.1			21	17.5	7.5
	20	26.7	8.1		6	24.6	7.8			22	17.8	7.5
	21	26.3	8.1		7	23.2	8.3			23	17.8	7.5
	22	26.1	8.3		. 8	22.3	8.3			24	17.5	7.5
	8.3				9	22.3	7.7			25	16.4	7.5
	24	25.6	8.3		10	22.8	8.1			26	17.4	7.0
	25	26.3	8.4		11	21.1	7.8			27	18.5	7.0
	26	26.5	8.5		12	21.1	8.1		·	28	17.5	7.3
	27	27.3	8.5		13	21.0	7.8			29	17.4	7.5
	28	27.0	8.3		14	21.7	7.9] [30	17.0	7.5
	29	26.7	8.4		15	22.1	7.9		Dec-12	1	13.7	8.1
	30	27.2	8.0		16	21.1	8.1			2	13.7	8.2
	31	27.0	8.3		17	20.5	7.9	<u> </u>		3	16.2	8.4
Sep-12	1	27.8	8.4		18	21.2	8.4	l L		4	16.8	8.4
	2	26.7	8.0		19	21.4	8.0	_		5	16.5	8.3
	3	27.5	7. 9	ļ ļ	20	21.1	8.1	l L		6	15.6	8.4
	4	26.8	7.8		21	21.3	8.1	ļ L		7	15.9	8.5
	5	27.6	8.0	<u> </u>	22	21.3	8.4	ļ ļ		8	16.8	8.3
	6	27.5	8.2		23	21.0	8.2	ļ <u>L</u>		9	17.8	8.0
	7	27.4	8.1		24	21.8	8.6	↓		10	16.8	8.2
	8	27.4	8.1		25	21.5	8.0	↓		11	16.4	8.3
	9	26.6	8.1		26	22.0	8.1	-		12	16.2	8.1
	10	25.9	8.1		27	22.0	8.1	-		13	15.4	8.3
	11	23.5	8.4		28	22.2	7.9	-		14	14.8	8.0
ļ	12				29	20.0	8.1	-		15	14.0	8.2
	13	25.0	8.0	<u> </u>	30	15.9	7.2	-		16	15.2	8.1
	14	24.4	7.9		31	17.1	8.1			17	15.9	8.3
	15	25.0	7.9	Nov-12	1	17.6	7.5			18	16.2	8.3
	16	23.8	8.4		2	16.9	7.5	L		19	15.7	82
	17	24.9	8.3		3	17.3	7.5			20	15.0	8.2
	18	25.1	8.1		4	18.3	7.0	J L		21	15.2	8.0

1	,	•	T
Month/ Year	Day	Temp °C	pΗ
	22	14.6	8.2
	23	13.2	8.4
	24	13.4	8.0
	25	13.7	8.0
	26	13.0	7.9
	27	12.3	8.2
	28	12.0	8.0
	29	11.8	8.1
	30	10.9	8.1
	31	10.3	7.9
Jan-13	1	10.3	7.9
	2	10.6	7.9
	3	9.9	7.9
	4		
	5	8.1	7.5
	6	9.4	7.8
	7	10.8	7.8
	8	10.9	7.8
	9	10.2	7.8 .
	10	10.7	7.9
	11	11.6	8.1
	12	12.2	8.2
	13	13.8	8.2
	14	15.0	7.9
	15	13.6	8.4
	16	13.6	7.9
	17	13.6	7.9
	18	11.9	8.0
	19	11.5	8.1
	20	11.9	8.1
	21	12.5	7.9
	22	11.7	8.0
	23	10.7	7.8
	24	10.8	7.7
	25	10.1	8.1
	26	10.1	7.9
-	27	10.4	7.6
	28	10.8	7.8
	29	11.5	7.8
	30	12.9	8.0
	31	13.0	7.6
Feb-13	1	11.9	8.1
	_ 2	11.0	8.0
	3	11.5	8.3
	4	10.7	8.1
	5	10.9	7.6
	6 .	11.2	7.8

Month/			
Year	Day	Temp °C	рН
	7	11.6	7.9
	8	12.2	8.0
	9	11.6	7.7
	10	10.7	8.3
	11	12.4	8.2
	12	12.9	8.1
	13	12.1	7.7
,	14	11.1	8.2
	15	12.2	8.2
	16	12.9	8.1
	17	11.8	8.1
	18	11.2	8.1
	19	11.0	7.6
	20	11.3	7.7
	21	10.9	7.9
	22	10.9	8.1
	23	11.4	7.9
	24	12.3	7.8
	25	11.7	8.3
	26	11.9	8.0
	27	12.0	8.0
	28	12.3	7.7
Mar-13	1	12.2	8.2
	2	12.3	8.1
	3	11.9 11.5	7.7 8.3
	5	12.2	
	6	9.8	7.7 8.2
	7	11.1	7.6
	8	10.9	7.8
	9	11.0	8.1
	10	12.0	7.7
	11	13.1	7.4
	12	13.7	7.5
	13	13.4	7.5
	14	13.4	7.4
	15	12.5	8.1
	16	13.1	7.8
	17	14.2	7.7
	18	13.6	7.7
	19	13.4	7.6
	20	13.4	7.5
	21	13.4	7.7
	22	12.6	7.7
	23	12.9	7.2
	24	13.3	7.7
	25	13.4	8.5

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Month/ Year	Day	Temp °C	рН
	26	13.3	7.7
	27	12.8	7.8
	28	12.9	7.6
	29	13.2	7.7
	30	13.0	7.6
	31	13.1	7.6
Apr-13	1	14.8	7.8
	2	13.7	7.3
	3		
	4	13.3	7.0
	5	14.7	7.7
	6	13.9	7.4
	7	14.4	7.7
	8	15.8	7.8
	9	16.8	7.7
	10	18.7	7.4
	11	19.2	6.9
	12	19.2	7.4
	13	19.2	7.3
	14	18.9	7.2
	15	18.5	8.7
	16	19.1	7.1
	17	20.0	7.6
	18	19.9	7.5
	19	20.3	7.8
	20	19.8	8.0
	21	18.7	7.8
	22	18.1	7.9
	23	18.4	7.6
	24	19.1	7.8
	25	18.5	7.8
	26	19.0	7.4
	27	19.0	7.7
	28	19.4	7.9
	29	18.5	8.0
	30	19.6	7.9
May-13	1	19.9	7.7
	2	19.9	7.1
	· 3	19.8	7.5
	4	19.6	7.3
	5	19.8	7.6
	6	20.1	7.4
	7	20.3	6.8
	- 8	20.4	6.8
	9	19.9	7.3
	10	20.4	7.3
	11	21.5	7.6

Month/ Year	Day	Temp °C	рН
	12	21.3	7.7
	13		
	14	20.7	7.6
	15	20.2	7.5
	16	21.4	7.4
	17	22.0	7.2
	18	22.1	7.3
	19	22.1	7.3
	20	22.8	7.1
	21	23.1	7.7
	2 2	24.0	7.5
	23	24.3	7.4
	24	23.1	7.4
	25	21.2	8.0
	26	21.4	8.1
	27	21.1	7.7
	28	21.9	7.5
	29	22.4	7.6
	30	23.6	7.5
	31	24.2	8.3
Jun-13	1	24.4	7.7
	2	24.8	7.7
	3	24.7	7.2
	4	24.3	8.0
	5	24.2	8.0
	6	23.5	8.1
	7	23.2	7.9
	8	23.4	8.1
	9	23.7	7.8
	10	23.6	7.7
	11	24.2	7.5
	12	24.5	7.4
	13	24.6	7.7
	14	23.6	7.6
	15	24.5	7.8
	16	24.8	7.7
ļ	17	24.5	7.8
<u> </u>	18	24.7	7.8
	19	24.6	8.2
	20	24.8	8.0
	21	24.4	8.0
	22	24.6	7.9
	23	25.3	7.6
	24	26.3	7.7
	25	26.9	8.1
<u> </u>	26	26.7	7.7
	27	26.1	7.7

Month/		_	
Year	Day	Temp °C	pН
	28	26.0	7.6
	29	25.7	7.7
	30	26.2	7.6
Jul-13	1	26.3	7.4
	2	26.7	7.7
	3	26.2	7.7
	4	26.6	7.7
	5	26.4	8.3
	6	27.5	8.1
	7	27.2	7.8
	8	26.7	7.8
	9	27.6	8.3
	10	27.2	7.8
	11	27.4	7.7
	12	26.1	7.7
	13	26.4	8.0
	14	26.8	8.0
	15	26.3	7.7
	16	27.6	7.9
	17	26.5	7.7
	18	28.2	7.8
	19	28.0	8.0
	20	28.1	7.9
	21	28.0	7.9
	22	27.2	7.9
	23	27.9	7.9
	24	27.4	7.8
	25	27.0	8.3
	26	· · · ·	
	27	26.0 26.3	8.0 7.7
	28	26.3	8.0
	29	26.2	7.6
	30	26.2	7.5
	31	26.0	7.9
Aug-13	1	26.5	8.0
₽.12	2	25.8	7.9
	3	26.3	8.0
	4	26.1	8.2
	5	25.7	8.3
	6	25.9	8.0
	7	26.3	8.0
	8	26.4	8.1
	9		
		26.3	8.0
	10	27.0	8.0
	11	26.9	8.3
	12	22.1	7.9
	13	27.0	8.3

B.d Ab. /	/		1
Month/ Year	Day	Temp °C	рН
	14	26.6	7.9
	15	25.7	8.3
	16	24.9	8.4
	17	25.2	8.5
	18	25.0	8.4
	19	25.2	7.6
	20	25.8	8.3
	21	26.4	8.0
	22	26.5	7.9
	23	25.8	8.4
	24	25.4	8.1
	25	25.1	8.4
	26	24.8	8.4
	27	26.3	8.3
	28	26.2	8.3
	29	26.0	8.1
	30	26.0	8.3
	31	26.5	8.3
Sep-13	1	26.8	8.3
	2	27.0	7.9
	3	27.3	8.4
	4	26.9	8.0
	5	26.4	8.1
	6	25.6	8.1
	7	25.0	8.4
	8	25.5	8.3
	9	25.6	8.1
	10	26.7	8.0
	11	27.4	8.5
	12	26.8	8.3
	13	26.1	8.2
	14	24.9	8.5
	15	24.4	8.4
	16	24.0	8.3
	17	24.0	8.3
	18	23.5	8.1
	19	23.4	8.2
 	20	22.9	8.3
	21	23.7	8.1
-	22	23.6	8.1 8.3
	23	234 22.9	8.1
	25	22.3	0.1
	26	72.6	8.1
	27	22.6	8.0
	28	22.7	8.2
	29	22.6	8.0
<u>l</u>	£3	22.0	6.0

Month/	_	T	
Year	Day	Temp °C	ρН
-	30	22.6	7.7
Oct-13	1	22.6	8.0
	2	23.6	8.1
	3	23.6	8.2
	4	22.7	8.1
	5	23.9	8.4
	6	24.0	7.5
	7	24.1	8.0
	8	22.6	8.0
	9	22.7	8.1
	10	21.5	8.1
	11	21.4	8.2
	12	22.0	8.1
	13	22.0	8.1
	14	22.6	8.0
	15	22.3	7.9
	16	22.7	8.3
	17	22.9	8.0
	18	21.8	8.0
	19	21.7	7.9
	20	21.5	8.1
	21	20.9	7.9
	22	20.7	8.2
	23	19.2	8.3
	24	19.4	8.2
	25	18.1	8.4
	26	18.4	8.3
	27	18.7	8.3
	28	17.5	8.5
	29	18.8	8.1
	30	18.9	8.3
	31	19.5	8.3

Temperature 90th Percentile = 26.9°C

pH 90th Percentile = 8.3 SU

pH 10th Percentile = 7.3 SU

Crowther, Joan (DEQ)

From: Aschenbach, Ernie (DGIF)

Sent: Thursday, August 22, 2013 4:16 PM

To: Crowther, Joan (DEQ): nhreview (DCR); susan_lingenfelser@fws.gov; Daub, Elleanore (DEQ)

Cc: ProjectReview (DGIF); Cason, Gladys (DGIF)

Subject: ESSLog 34063, VPDES Permit# VA0077411 Re-issuance for the Fauquier Springs WWTP

near Warrenton, VA

We have reviewed the VPDES re-issuance for the above-referenced facility. The receiving stream is the Rappahannock River. The current design flow of the facility is 0.01 MGD with plans to expand to 0.02 MGD under the new permit. The receiving stream has a low-flow 7Q10 of 1.7 million gallons per day (MGD), and high-flow 7Q10 of 21 MGD. The existing Ammonia as Nitrogen from (monthly-average) is 16 mg/L, and (weekly-average) is 16 mg/L. The proposed Ammonia as Nitrogen will remain the same. The total residual Chlorine (monthly-average) is 0.70 mg/L, and (weekly-average) is 0.090 mg/L (after dechlorination) and will remain the same under the new permit.

According to our records, the Rappahannock River is a designated Threatened and Endangered (T&E) species water for the state Threatened (ST) green floater mussel. It is also predicted habitat for the federal Endangered state Endangered (FESE) dwarf wedgemussel.

In order to protect aquatic resources, we generally recommend ultraviolet (UV) disinfection rather than chlorination disinfection. If chlorination becomes necessary and is used, we recommend and support continued dechlorination, prior to discharge. The ammonia limits proposed within the EPA rule are expressed on the basis of total ammonia-nitrogen (TAN). The proposed EPA ammonia limit for waters with mussels (not T&E mussels, <u>any</u> mussel species) is:

- CMC (Criterion Maximum Concentration or acute) 2.9 mg N/L (at pH 8 and 25C)
- CCC (Criterion Continuous Concentration or chronic) 0.26 mg N//L (at pH 8 and 25C) with a 4-day average within the 30 day average period no higher than 2.5 the CCC, which would be 0.65 mg N/L.

The ammonia limits proposed within the EPA rule are the best information currently available regarding ammonia levels protective of mussels. Therefore, we recommend and support the EPA values being implemented in this permit for this and all future VPDES permits.

This project is located within 2 miles of a documented occurrence of a state or federal threatened or endangered plant or insect species and/or other Natural Heritage coordination species. Therefore, we recommend and support coordination with VDCR-DNH regarding the protection of these resources. We also recommend contacting the USFWS regarding all federally listed species.

Thank you for the opportunity to provide comments. Please call me if you have any questions.

Ernie Aschenbach Environmental Services Biologist Virginia Dept. of Game and Inland Fisheries P.O. Box 11104 4010 West Broad Street Richmond, VA 23230 Phone: (804) 367-2733

FAX: (804) 367-2427

Email: Ernie.Aschenbach@dgif.virginia.gov

Mixing Zone Predictions for

Fauquier Springs 7Q10

Effluent Flow = .02 MGD Stream 7Q10 = 1.68 MGD Stream 30Q10 = 3.6 MGD Stream 1Q10 = 1.42 MGD Stream slope = 0.006 ft/ft Stream width = 50 ft Bottom scale = 1 Channel scale = 1

Mixing Zone Predictions @ 7Q10

Depth = .1036 ft Length = 34637.27 ft Velocity = .5079 ft/sec Residence Time = .7894 days

Recommendation:

A complete mix assumption is appropriate for this situation and the entire 7Q10 may be used.

Mixing Zone Predictions @ 30Q10

Depth = .1633 ft Length = 23678.67 ft Velocity = .6865 ft/sec Residence Time = .3992 days

Recommendation:

A complete mix assumption is appropriate for this situation and the entire 30Q10 may be used.

Mixing Zone Predictions @ 1Q10

Depth = .0938 ft Length = 37646.87 ft Velocity = .4753 ft/sec

Residence Time = 22.0008 hours

Recommendation:

A complete mix assumption is appropriate for this situation providing no more than 4.55% of the 1Q10 is used.

------ Attachment 8

Mixing Zone Predictions for

Fauquier Springs High Flows

Effluent Flow = .02 MGD Stream 7Q10 = 21.3 MGD Stream 30Q10 = 30.4 MGD Stream 1Q10 = 16.8 MGD Stream slope = .006 ft/ft Stream width = 50 ft Bottom scale = 1 Channel scale = 1

Mixing Zone Predictions @ 7Q10

Depth = .4754 ft Length = 9637.48 ft Velocity = 1.3885 ft/sec Residence Time = .0803 days

Recommendation:

A complete mix assumption is appropriate for this situation and the entire 7Q10 may be used.

Mixing Zone Predictions @ 30Q10

Depth = .5894 ft Length = 8032.53 ft Velocity = 1.5978 ft/sec Residence Time = .0582 days

Recommendation:

A complete mix assumption is appropriate for this situation and the entire 30Q10 may be used.

Mixing Zone Predictions @ 1Q10

Depth = .4119 ft Length = 10877.7 ft Velocity = 1.2641 ft/sec Residence Time = 2.3903 hours

Recommendation:

A complete mix assumption is appropriate for this situation providing no more than 41.84% of the 1Q10 is used.

The Water Quality S lard requirement for Ammonia is endent on the stream's temperature and pH. The temperature and pH data used to determine the Ammonia effluent limitations was collected at River Mile 147.1 on the Rappahannock River This is approximately 11.2 miles downstream from the discharge. This data was collected between July, 1968 and February, 1993. The temperature's 90th percentile is 25°C and the pH 90th percentile is 7.8 SU. See attached sheets for Total Ammonia Value Calculations.

ACUTE AMMONIA STANDARD FOR FRESHWATER: WARM WATER HABITATS, TROUT OR OTHER SENSITIVE COLDWATER SPECIES ABSENT, (TOTAL AMMONIA VALUE IS BASED ON THE WATER QUALITY STANDARDS (VR680-21-01.14.B):

TOTAL AMMONIA: 9.37 MG/L

 $N-NH_{\tau}$: 9.37 x 0.824 = 7.7 MG/L

CHRONIC AMMONIA STANDARD FOR FRESHWATER: WARM WATER HABITATS, TROUT OR OTHER SENSITIVE COLDWATER SPECIES ABSENT, (TOTAL AMMONIA VALUE IS BASED ON THE WATER QUALITY STANDARDS (VR680-21-01.14.B):

TOTAL AMMONIA: 1.5 MG/L

 $N-NH_3$: 1.5 x 0.824 = 1.24 MG/L

FAUQUIER SPRINGS COUNTRY CLUB STP, VPDES PERMIT NO. VA0077411

CALCULATION FOR TOTAL AMMONIA VALUES AT DIFFERENT ph'S AND TEMPERATURE THAN LISTED IN THE WATER QUALITY STANDARDS (VR680-21-01.14B)

pH = 7.8 standard units temperature = 25°C

THE ONE HOUR AVERAGE CONCENTRATION OF AMMONIA (IN MG/L AS UN-IONIZED NH₃) CAN BE CALCULATED BY USING THE FOLLOWING FORMULAS.

Acute criteria concentration = 0.52/FT/FPH/2

where: FT - Final Temperature

 $FT = 10^{0.03(20 - TCAP)}$; $TCAP < T < 30^{\circ}C$

TCAP = 25°C; when trout and other sensitive coldwater species are absent

 $FT = 10^{0.03(20-25)}$

FT = 0.7079

where: FPH = Final pH

$$FPH = \frac{(1 + 10^{(7.4 - pH)})}{1.25}$$
; 6.5 < pH < 8.0

$$FPH = \frac{(1 + 10^{(7.4 - 7.8)})}{1.25}$$

FPH = 1.12

Therefore:

ACUTE CRITERIA CONCENTRATION = 0.52/0.7079/1.12/2 = 0.3279

CONVERSION FROM UN-IONIZED TO TOTAL AMMONIA CAN BE CALCULATED BY USING THE FOLLOWING FORMULAS.

TOTAL AMMONIA CRITERIA = CALCULATED UN-IONIZED AMMONIA CRITERIA DIVIDED BY FRACTION OF UNIONIZED AMMONIA

Where: Fraction of un-ionized ammonia = $1/(10^{p\text{Ka-pH}} + 1)$

where: pKa = 0.09018 + (2729.92/(273.2 + temperature °C))pKa = 9.24

Fraction of un-ionized ammonia = 0.035

THEREFORE: TOTAL ACUTE AMMONIA CRITERIA = CALCULATED UN-IONIZED AMMONIA CRITERIA DIVIDED
BY FRACTION OF UN-IONIZED AMMONIA

TOTAL ACUTE AMMONIA CRITERIA = 0.3273/0.035 = 9.37 mg/l

THANKS - DISCUSSOR COOKING CHOD DIT! ASDED SUMMER! - AUGOSTATI

CALCULATION FOR TOTAL AMMONIA VALUES AT DIFFERENT pH'S AND TEMPERATURE THAN LISTED IN THE WATER QUALITY STANDARDS (VR680-21-01.14B)

pH = 7.8 standard units temperature = 25°C

THE 4-DAY AVERAGE CONCENTRATION OF AMMONIA (IN MG/L AS UN-IONIZED NH_3) CAN BE CALCULATED BY USING THE FOLLOWING FORMULAS.

Chronic criteria concentration = 0.8/FT/FPH/RATIO

where: FT = Final Temperature

 $FT = 10^{0.03(20 - TCAP)}; TCAP < T < 30^{\circ}C$

TCAP = 20°C; when trout and other sensitive coldwater species are absent

 $FT = 10^{0.03(20 - 20)}$

FT = 1

where: FPH = Final pH

 $PPH = \frac{(1 + 10^{(7.4 - pM)})}{1.25}$; 6.5 < pH < 8.0

 $FPH = \frac{(1 + 10^{(7.4 - 7.8)})}{1.25}$

FPH = 1.12

RATIO = 13.5; 7.7 < pH < 9

Therefore:

CHRONIC CRITERIA CONCENTRATION = 0.8/1/1.12/13.5 = 0.0529

CONVERSION FROM UN-IONIZED TO TOTAL AMMONIA CAN BE CALCULATED BY USING THE FOLLOWING FORMULAS.

TOTAL CHRONIC AMMONIA CRITERIA - CALCULATED UN-IONIZED AMMONIA CRITERIA DIVIDED BY FRACTION OF UN-IONIZED AMMONIA

Where: Fraction of un-ionized ammonia = 1/(10pKa-pR + 1)

where: pKa = 0.09018 + (2729.92/(273.2 + temperature °C))

pKa = 9.24

Fraction of un-ionized ammonia = 0.035

THEREFORE: TOTAL CHRONIC AMMONIA CRITERIA = CALCULATED UN-IONIZED AMMONIA CRITERIA
DIVIDED BY FRACTION OF UN-IONIZED AMMONIA

TOTAL CHRONIC AMMONIA CRITERIA - 0.0529/0.035 - 1.5 mg/l

THE INSTREAM WASTEWATER CONCENTRATION (IWC) CALCULATION: This calculation expresses the percentage of wastewater in the mix of wastewater and the receiving stream.

$$IWC % = \frac{Q_e}{(Q_e + Q_e)}$$
 (100)

where:

 $\mathbf{Q_s}$ = critical receiving stream flow $\mathbf{Q_e}$ = design flow for facility

Definitions for types of critical receiving stream flow (Q_c) :

1010 is the critical receiving stream flow used to determine acute aquatic life standard. 1010 is defined as the lowest steam flow which on a statistical basis, would occur for a 1-day period once every 10 years.

7010 is the critical receiving stream flow used to determine chronic aquatic life standard. 7010 is defined as the lowest steam flow which on a statistical basis, would occur for a 7-consecutive-day period once every 10 years.

3005 is the critical receiving stream flow used to determine non-carcinogenic human healt standards. 3005 is defined as the lowest stream flow which on a statistical basis, would occur for a 30-consecutive-day period once every 5 years.

The harmonic mean is the critical receiving stream flow used to determine carcinogenic human health standards. Harmonic mean is defined as the reciprocal of the arithmetic mea of the flow reciprocals.

The critical receiving stream flows for this discharge are as follows:

1010 = 1.42 MGD

7Q10 = 1.68 MGD

3005 = 6.2 MGD

Harmonic Mean = 25.2 MGD

Acute IWC =
$$\frac{0.01743}{(0.01743 + 1.42)}$$
 (100) =1.2%

Chronic IWC =
$$\frac{0.01743}{(0.01743 + 1.68)}(100) = 1.07\%$$

THE WASTELOAD ALLOCATION FOR AMMONIA:

$$WLA = \frac{C_o(Q_o + Q_s) - (C_s)(Q_s)}{Q_s}$$

where:

WLA = wasteload allocation

 Q_s = critical receiving stream flow

Q = design flow

 C_0^e = in stream standard C_s = mean background concentration of parameter in stream

ACUTE WLA (WLA,):

For stream dominated dischargers (defined as in IWC of 50% or less at critical

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Page 6

conditions), a steady state complete mix equation could result in a relatively large WLA_a. It is believed that discharges containing this large WLA_a could result in an introduction of concentrations of pollutants into the receiving stream that would not completely mix in a relatively rapid manner and may possibly cause lethality in the allocated impact zone. In order to ensure protection against lethality, the WLA_a for discharges into these stream dominated situations are set at 2 times the acute standard. The 2X factor is derived from the fact that the acute standard (or Criteria Maximum Concentration - CMC) is defined as one half of the final acute value (FAV) for a specific toxic pollutant. The term "final acute value" is defined as a cumulative probability of 0.05 for the acute toxicity values for all genera for which acceptable acute tests have been conducted with toxicant.

$$WLA_{a} = (7.7)(2) = 15.4 \text{ mg/}1$$

CHRONIC WLA (WLA_)

For stream dominated situations, a steady state complete mix with the whole 7Q10 is believed to be acceptable. This is because lethality in the allocated impact zone is addressed by the WLA₈ so the zone of passage restrictions are the remaining restrictions to be addressed. It is believed that since the ratio of stream flow to effluent flow is relatively large, the effluent plume should not extend across the width of the stream prior to complete mix. This characteristic should allow the movement of passing or drifting organisms by the effluent plume, and it is assumed in accordance with VR680-21-01.4.a. that the complete mix is appropriate for addressing the spatial requirements.

$$WLA_c = \frac{C_o(Q_s + Q_o)}{Q_o} \qquad where C_s = 0.0 mg/1$$

$$WLA_c = \frac{1.24 (1.68 + 0.01743)}{0.01743}$$

 $WLA_c = 120.8 \, mg/l$

Based on the above information, a computer program (attached) was utilized to develop the ammonia effluent limitations. The program uses methods described in Appendix E of the USEPA Technical Support Document for Water Quality Based Toxics Control, (1991). The ammonia effluent limitations for this discharge are:

Maximum Daily Limit: 15.4 mg/l

Average Monthly Limit: 15.4 mg/l

Analysis of the Fauquier Springs Country Club STP effluent data for Ammonia

The statistics for Ammonia are:

Number of values = 1

Detection = .1 mgil

Number < detection = 0

Expected value = 7.253759 = 18.94322 Variance

. 6 C.V.

97th percentile = 17.65175 Statistics used = Reasonable potential assumptions

The WLAs for Ammonia are:

Acute WLA = 15.4 ms/l Chronic WLA = 120.8 mg/L Human Health WLA = ----

The limits are based on acute toxicity and 1 samples/month.

Maximum daily limit = 15.4 mg/1 Average monthly limit = 15.4 mg/l

DATA 6.22

TEMPERATURE AND PE FOR RAPPAHANHOCK RIVER AT RIVER MILE 147.1

Data from July, 1968 through February, 1993

Temperature	Sorted Temperature	₽Ħ	Sorted pH	
27.8	29	7.5	9.2	
25.6	28.3	7.8	9	
20	- 28.3	6.5	9	90th Percentile for Temperature
15	28.2	6.5	8.7	·
3.3	28	6.8	8.7	251 values
20	27.8	6.5	8.4	251 x 0.9 = 225.9 = 226
22.2	27.8	6.5	8.33	Temperature 90th percentile = 25 C
2.8	27.7	6.8	8.2	•
8.3	27	6.7	8.1	•
13.3	27	6.8	8.1	
20.6	26.7	7	8.1	90th Percentile for pH
23.9	26.5	6.8	8.1	•
22.8	26.5	6.8	8.1	246 values
17.2	26.4	9	8.1	246 x 0.9 = 221.4 = 221
3.9	26	6.2	8	pH 90th percentile = 7.8 su
₂ 3.3	26	6.5	8	
4.4	26	7	8	
7.2	26	7.5	8	•
13.3	26	7.5	8	
13.9	25.7	7.5	8	•••
17.8	25.6	7	8	
25.6	25.6	7.8	7.9	
22.2	25.6	7.7	7.9	
16.7	25.6	7	7.9	
21.1	25.5	7.1	7.8	
7.8	25	9.2	7.8	
8.9	25	6.8	7.8	•
6.1	25	1.7	7.8	
2.2	24.7	6.8	7.7	·
11.1	24.7	6.5	1.1	
10.6	24.4	7. f	1.1	
17.8	24.2	1	7.7	•
21.1	24	7	1.1	•
25.6	24	7.2	1.1	
22.8	23.9	7	7.7	
17.2	23.9	6.7	7.7	
16.1	23.9	7.2	7.7	
9.4	23.8	6.8	7.7	
5.6	23.5	7	7.7	
6.7	23.5	7	7.6	•
3.9	23.5	6.8	7.6	
12.2	23	6.7	7.6	
8.9	23	6.8	7.6	
17.8	22.8	7	7.6	
27.8	22.8	1.2	7.6	
22.2	22.7	7	7.6	
17.2	22.7	7.2	7.6	
8.3	22.5	7	7.6	
10	22.2	6.5	7.6	•
6.7	22.2	5.9	7.6	
1.7	22.2	7.5	7.55	
14.4	22.2	7.2	7.5	

FAUQUIER SPRINGS COUNTRY CLUB STP-VA0077411 EFFLUENT MONITORING DATA FOR AMMONIA AS NITROGEN JANUARY 1994 TO APRIL 1998

DATE	AMMONIA
JANUARY 1994	12.4
FEBRUARY 1994	9.47
MARCH 1994	4.8
APRIL 1994	4.3
MAY 1994	8.4
JUNE 1994	11.1
JULY 1994	4.7
AUGUST 1994	6.5
SEPTEMBER 1994	10.6
OCTOBER 1994	10.7
NOVEMBER 1994	11.5
DECEMBER 1994	13.9
JANUARY 1995	15.6
FEBRUARY 1995	15.6
MARCH 1995	12.8
APRIL 1995	0.1
MAY 1995	14.4
JULY 1995	12.6
AUGUST 1995	7
SEPTEMBER 1995	6.4
OCTOBER 1995	5.7
NOVEMBER 1995	3.5
DECEMBER 1995	4.1
JANUARY 1996	2.9
FEBRUARY 1996	1.1
MARCH 1996	1
MARCH 1996	7.4
APRIL 1996	5.8
MAY 1996	8.7
JUNE 1996	7.1
JULY 1996	9.6
AUGUST 1996	10.9
SEPTEMBER 1996	1
OCTOBER 1996	0.5
NOVEMBER 1996	0.2
DECEMBER 1996	0.4
JANUARY 1997	0.1
FEBRUARY 1997	0.5
MARCH 1997	0.5
APRIL 1997	0.7

DATE	AMMONIA
MAY 1997	4.1
JUNE 1997	7.6
JULY 1997	13
AUGUST 1997	8.8
SEPTEMBER 1997	1
OCTOBER 1997	0.8
NOVEMBER 1997	0.4
DECEMBER 1997	2.2
JANUARY 1998	1.5
FEBRUARY 1998	3.6
MARCH 1998	3.1
APRIL 1998	3.5

Permit Limit Effective Date

Facility = Fauquier Springs CC STP (VA0077411) Chemical = Ammonia as Nitrogen Chronic averaging period = 30 WLAa = 15.6WLAc = 37.8Q.L. = 0.2# samples/mo. = 1 # samples/wk. = 1Summary of Statistics: # observations = 1 Expected Value = 9 Variance = 29.16C.V. = 0.697th percentile daily values = 21.9007 97th percentile 4 day average = 14.9741 97th percentile 30 day average= 10.8544 # < Q.L. = 0 Model used = BPJ Assumptions, type 2 data

A limit is needed based on Acute Toxicity
Maximum Daily Limit = 15.6
Average Weekly limit = 15.6
Average Monthly Llmit = 15.6

The data are:

9

Criteria and WLA Calculations for Ammonia based upon freshwater criteria (Nontidal Only)

Facility: Fauquier Springs Country Club STP

Permit Number: VA0077411

Comments: 3-RPP147.10 pH and Temp Data 1993-2003

pH	=	7.80	S.U.	
Temperature	=	24.70	°C	
1Q10	Ξ	1.422	MGD	
7Q10	=	1.680	MGD	
30Q5	=	6.14	MGD	
Harmonic Mean	=	25.00	MGD	
Design Flow	= .	0.02	MGD	
Percentage of 1Q10 by MIX.exe	=	9.27%	0.132	MGD
Percentage of 7Q10 by MIX.exe	=	100.00%	NA	MGD
Water Body Tier	=	2	(1=No Antideg; 2=	Antideg)

Final Temperature (FT) Final Temperature (FT)	==	10 ^{(0.03)(20-} 0.723	-т,	Final Temperature (FT) Final Temperature (FT)	=======================================	10 ^(0.03) (2 ⁰⁻¹⁷⁾ 0.723
Final pH (FPH)	=		8.0 <ph<9.0< td=""><td>Final pH (FPH)</td><td>=</td><td>1; where 8.0<ph<9.0< td=""></ph<9.0<></td></ph<9.0<>	Final pH (FPH)	=	1; where 8.0 <ph<9.0< td=""></ph<9.0<>
or	=	(1+10 ^{(7.4-}	^{pH)})/1.25; where 6.5 <ph<8.0< td=""><td>or</td><td>=</td><td>(1+10^(7,4-pH))/1.25; where 6.5<ph<8.0< td=""></ph<8.0<></td></ph<8.0<>	or	=	(1+10 ^(7,4-pH))/1.25; where 6.5 <ph<8.0< td=""></ph<8.0<>
Final pH (FPH)	=	1.118	•	Final pH (FPH)	=	1.118
Calculated Unionized Ammonia	=	((0.52/FT	Г)/FPH)/2	Ratio	=	13.5; where 7.7 <ph<9.0< td=""></ph<9.0<>
Calculated Unionized Ammonia	=	0.3216	•	or	=	[(20.25)(10 ^(7,7-pH))]/(1+ 10 ^(7,4-pH)); where 6.5 <ph<7.7< td=""></ph<7.7<>
		3,32.3		Ratio	=	13.500
рКа	=	0.09018	+ (2729.92/(273.2 + Temp.))			
pKa	=	9.254	(**************************************	Calculated Unionized Ammonia	=	((0.8/FT)/FPH)/Ratio
Fraction of Unionized Ammonia	=	1/(10 ^{(pKa-}	^{pH)} +1)	Calculated Unionized Ammonia	=	0.0733
Fraction of Unionized Ammonia	=	0.0340	• • • • • • • • • • • • • • • • • • • •	Octobiated Dinotile 22 / Millionia		
Traction of Chichices / Whitehild	_	0.0040		рКа	=	0.09018 + (2729.92/(273.2 + Temp.))
Total Acute Ammonia Criteria	=	9.471	mg/I as NH ₃	pKa	=	9.254
		-	•	·		1/(10 ^(pKa-pH) +1)
Total Acute Ammonia Criteria	=	7.80	mg/I as N	Fraction of Unionized Ammonia	=	· · · · · · · · · · · · · · · · · · ·
				Fraction of Unionized Ammonia	=	0.0340
				Total Acute Ammonia Criteria	=	2.159
			•	Total Acute Ammonia Criteria	=	1.78

					Antideg					Antideg	
		Acute	Acute	Acute	Acute	SSTV =	Chronic	Chronic	Chronic	Chronic	SSTV =
	Instream	Criteria	Baseline	WLA	WLA	0.4 X aWLA	Criteria	Baseline	WLA	WLA	0.6 X cWLA
Parameters	Background	(mg/l)	(mg/l)	(mg/l)	(mg/l)	(mg/l)	(mg/l)	(mg/l)	(mg/l)	(mg/l)	(mg/l)
Ammonia	ND	7.80	1.95	59.24	140.67	23.70	1.78	0.44	151.19	37.80	22.68

Notes:

- 1) ND = No Data available, and therefore the background concentrations are assumed to be Zero.
- 2) Total Ammonia Criteria (Acute & Chronic) = Calculated un-ionized ammonia criteria divided by fraction of un-ioized Ammonia
- 3) Total Ammonia is then converted to Ammonia-Nitrogen by multiplingTotal Ammonia by 0.824
- 4) In the pKa calculation the temperature is °C.
- 5) Acute criteria/WLA based on 1Q10 flow; chronic criteria/WLA based on 7Q10 flow.

Mixing Zone Predictions for Fauquier Springs High flow

Effluent Flow = 0.02 MGD Stream 7Q10 = 20.0 MGD Stream 30Q10 = 30.4 MGD Stream 1Q10 = 16.2 MGD Stream slope = .006 ft/ft Stream width = 50 ft Bottom scale = 3 Channel scale = 1

Mixing Zone Predictions @ 7Q10

Depth = .7376 ftLength = 3017.69 ftVelocity = .8402 ft/sec Residence Time = .0416 days

Recommendation:

A complete mix assumption is appropriate for this situation and the entire 7Q10 may be used.

Mixing Zone Predictions @ 30Q10

Depth = .9513 ft Length = 2427.33 ft Velocity = .99 ft/sec Residence Time = .0284 days

Recommendation:

A complete mix assumption is appropriate for this situation and the entire 30Q10 may be used.

Mixing Zone Predictions @ 1Q10

Depth = .6493 ft Length = 3363.23 ftVelocity = .7734 ft/sec Residence Time = 1.2079 hours

Recommendation:

A complete mix assumption is appropriate for this situation providing no more than 82.79% of the 1Q10 is used.

Mixing Zone Predictions for

Fauquier Springs CC STP

Effluent Flow = 0.02 MGD Stream 7Q10 = 1.68 MGD Stream 30Q10 = 3.6 MGD Stream 1Q10 = 1.422 MGD Stream slope = 0.006 ft/ft Stream width = 50 ft Bottom scale = 3 Channel scale = 1

Mixing Zone Predictions @ 7Q10

Depth = .1665 ft Length = 10589.3 ft Velocity = .3161 ft/sec Residence Time = .3877 days

Recommendation:

A complete mix assumption is appropriate for this situation and the entire 7Q10 may be used.

Mixing Zone Predictions @ 30Q10

Depth = .2624 ft
Length = 7228.07 ft
Velocity = .4271 ft/sec
Residence Time = .1959 days

Recommendation:

A complete mix assumption is appropriate for this situation and the entire 30Q10 may be used.

Mixing Zone Predictions @ 1Q10

Depth = .1508 ft Length = 11502.92 ft Velocity = .2961 ft/sec

Residence Time = 10.7926 hours

Recommendation:

A complete mix assumption is appropriate for this situation providing no more than 9.27% of the 1Q10 is used.

COUNT	DATE	рН	pH-Sort	DATE	TEMP C	Temp-Sort
1	5/29/2003	7.1	6.4	5/29/2003	15.4	0.1
2	2/11/2003	7.3	6.4	2/11/2003	1.5	0.5
3	1/30/2003	7.3	6.5	1/30/2003	0.1	1.0
4	6/6/2001	6.9	6.5	6/6/2001	25.8	1.3
5	5/1/2001	7.5	6.5	5/1/2001	16.5	1.5
6	4/3/2001	7.3	6.5	4/3/2001	8.5	2.4
7	11/1/2000	6.5	6.6	11/1/2000	11.4	3.0
8	10/3/2000	7.1	6.8	10/3/2000	17.1	3.0
9	9/13/2000	6.9	6.8	9/13/2000	22.1	3.1
10	8/8/2000	7.1	6.8	8/8/2000	24.7	3.2
11	7/12/2000	7.1	6.8	7/12/2000	23.0	3.3
12	6/13/2000	7.0	6.8	6/13/2000	22.3	3.8
13	5/4/2000	7.0	6.8	5/4/2000	19.5	3.8
14	4/12/2000	7.4	6.8	4/12/2000	15.2	3.8
15	3/23/2000	6.4	6.8	3/23/2000	10.8	3.9
16	2/10/2000	7.7	6.9	2/10/2000	1.3	3.9
17	1/12/2000	6.5	6.9	1/12/2000	4.8	4.5
18	12/13/1999	7.5	6.9	12/13/1999	4.5	4.8
19	10/6/1999	7.2	6.9	10/6/1999	14.2	5.0
20	9/8/1999	6.9	6.9	9/8/1999	22.8	5.8
21	8/17/1999	7.4	7.0	8/17/1999	28.8	6.0
22	7/20/1999	7.3	7.0	7/20/1999	27.0	6.7
23	6/22/1999	7.4	7.0	6/22/1999	21.9	7.0
24	5/13/1999	6.8	7.0	5/13/1999	19.8	7.1
25	3/16/1999	7.0	7.0	3/16/1999	3.8	7.3
26	1/13/1999	6.8	7.0	1/13/1999	1.0	7.6
27	12/16/1998	7.4	7.0	12/16/1998	3.8	7.7
28	11/18/1998	7.0	7.0	11/18/1998	8.0	7.9
29	10/22/1998	7.0	7.1	10/22/1998	11.4	8.0
30	9/16/1998	7.0	7.1	9/16/1998	24.7	8.5
31	8/19/1998	7.8	7.1	8/19/1998	23.6	9.8
32	7/21/1998	7.8	7.1	7/21/1998	26.3	10.2
33	6/25/1998	7.6	7.1	6/25/1998	24.1	10.4
34	5/12/1998	7.9	7.1	5/12/1998	14.7	10.8
35	4/29/1998	7.5	7.1	4/29/1998	14.3	11.4
36	4/9/1998	7.9	7.2	4/9/1998	13.8	11.4
37	3/18/1998	7.5	7.2	3/18/1998	5.8	11.5
38	2/26/1998	7.3	7.2	2/26/1998	7.9	11.6
39	1/21/1998	6.6	7.2	1/21/1998	3.3	13.0
40	12/17/1997	7.6	7.2	12/17/1997	3.2	13.4
41	11/18/1997	7.5	7.2	11/18/1997	3.9	13.4
42 43	10/8/1997	7.3	7.2	10/8/1997	19.2	13.7
43 44	9/10/1997 8/28/1997	7.5	7.3	9/10/1997	21.2	13.8
44 45	7/24/1997	7.5	7.3	8/28/1997	23.4	14.2
45 46	5/22/1997	7.6 7.1	7.3	7/24/1997	21.6	14.3
46 47			7.3	5/22/1997	17.2	14.7
	4/23/1997	7.2	7.3	4/23/1997	11.5	15.2
48 40	3/26/1997	7.1	7.3	3/26/1997	10.2	15.4
49 50	2/20/1997	7.6	7.3	2/20/1997	9.8	16.1
50 51	1/29/1997	7.0	7.3	1/29/1997	3.0	16.4
ŲΙ	12/18/1996	7.3	7.3	12/18/1996	7.7	16.5

P8586

52	11/20/1996	7.5	7.3	11/20/1996	7.6	17.1
53	9/26/1996	7.7	7.3	9/26/1996	16.4	17.2
54	8/27/1996	7.8	7.3	8/27/1996	23.6	18.2
55	7/24/1996	7.3	7.3	7/24/1996	23.4	18.3
56	6/27/1996	8.0	7.3	6/27/1996	22.8	19.2
57	6/21/1996	7.2	7.3	6/21/1996	24.1	19.5
58	5/21/1996	7.3	7.4	5/21/1996	23.5	19.8
59	4/15/1996	6.5	7.4	4/15/1996	13.7	20.5
60	3/21/1996	6.4	7.4	3/21/1996	6.7	21.2
61	2/22/1996	6.5	7.4	2/22/1996	7.0	21.4
62	11/8/1995	7.6	7.4	11/8/1995	7.3	21.6
63	8/23/1995	7.6	7.4	8/23/1995	24.1	21.9
64	7/20/1995	7.2	7.5	7/20/1995	25.5	22.1
65	6/21/1995	7.2	7.5	6/21/1995	24.0	22.3
66	5/24/1995	7.2	7.5	5/24/1995	21.4	22.8
67	4/26/1995	7.0	7.5	4/26/1995	13.4	22.8
68	3/23/1995	7.7	7.5	3/23/1995	10.4	23.0
69	2/14/1995	7.8	7.5	2/14/1995	0.5	23.1
70	1/25/1995	7.4	7.5	1/25/1995	3.0	23.4
71	12/20/1994	7.6	7.5	12/20/1994	3.8	23.4
72	10/18/1994	6.8	7.6	10/18/1994	11.6	23.5
73	9/8/1994	7.8	7.6	9/8/1994	18.2	23.6
74	8/11/1994	7.4	7.6	8/11/1994	25.7	23.6
75	7/19/1994	7.3	7.6	7/19/1994	23.9	23.6
76	6/2/1994	7.2	7.6	6/2/1994	20.5	23.8
77	5/12/1994	6.9	7.6	5/12/1994	16.1	23.9
78	3/17/1994	6.9	7.6	3/17/1994	5.0	24.0
79	2/17/1994	6.8	7.6	2/17/1994	2.4	24.1
80	11/22/1993	7.6	7.7	11/22/1993	6.0	24.1
81	. 10/7/1993	7.3	7.7	10/7/1993	13.4	24.1
82	9/7/1993	7.3	7.7	9/7/1993	23.6	24.7
83	8/12/1993	7.3	7.8	8/12/1993	23.8	24.7
84	7/15/1993	7.3	7.8	7/15/1993	26.7	25.5
85	6/17/1993	6.8	7.8	6/17/1993	23.1	25.7
86	5/17/1993	6.8	7.8	5/17/1993	18.3	25.8
87	4/19/1993	7.3	7.8	4/19/1993	13.0	26.3
88	3/22/1993	7.1	7.9	3/22/1993	7.1	26.7
89	2/23/1993	6.8	7.9	2/23/1993	3.9	27.0
90	1/26/1993	6.8	8.0	1/26/1993	3.1	28.8

Per bog 6

The regional modeling system has been used to 1) verify the adequacy of the current permit limits for the reissuance of Fauquier Springs Country Club and 2) to verify that antidegradation, a D.O. drop of not more than 0.2 mg/l, would not occur.

The model has been run from the discharge point of the proposed River Ridge Utility Company STP upstream of the Fauquier Springs Country Club STP to a point 3 miles downstream of the Fauquier Springs Country Club STP. The permit limits for the River Ridge Utility Company STP and the proposed South Wales STP were used to simulate background conditions for the river, once these facilities are constructed.

The TKN limit for Fauquier Springs Country Club STP was derived by doubling the facility's current ammonia as nitrogen limit of 15.4 mg/l, since the assumption is made that TKN is equal to twice the ammonia as nitrogen value.

REGIONAL MODELING SYSTEM VERSION 3.2

MODEL SIMULATION FOR THE River Ridge Utility Company STP DISCHARGE

TO Rappahannock River

THE SIMULATION STARTS AT THE River Ridge Utility Company STP DISCHARGE

FLOW = .05 MGD CBOD5 = 9 Mg/L TKN = 3 Mg/L D.O. = 5 Mg/L

**** THE MAXIMUM CHLORINE ALLOWABLE IN THE DISCHARGE IS 0.367 Mg/L ****

THE SECTION BEING MODELED IS BROKEN INTO 3 SEGMENTS RESULTS WILL BE GIVEN AT 0.1 MILE INTERVALS

THE 7010 STREAM FLOW AT THE DISCHARGE IS 1.62000 MGD

THE DISSOLVED OXYGEN OF THE STREAM IS 7.296 Mg/L

THE BACKGROUND CBODU OF THE STREAM IS 5 Mg/L

THE BACKGROUND nBOD OF THE STREAM IS 0 Mg/L

SEG.	LEN. Mi	VEL. F/S	K2 1/D	K1 1/D	KN 1/D	BENTHIC Mg/L	ELEV. Ft	TEMP.	DO-SAT Mg/L
1	2.10	0.816	8.571	0.500	0.150	0.000	335.00	26.00	8.106
2	1.90	0.753	6.316	0.500	0.150	0.000	310.00	26.00	8.113
3	3.00	0.522	3.000	0.500	0.150	0.000	292.50	26.00	8.118

(The K Rates shown are at $20\frac{1}{2}$ C ... the model corrects them for temperature.)

TOTAL STREAMFLOW = 1.6700 MGD (Including Discharge)

DISTANCE FROM HEAD OF SEGMENT (MI.)	TOTAL DISTANCE FROM MODEL BEGINNING (MI.)	DISSOLVED OXYGEN (Mg/L)	cBODu (Mg/L)	nBODu (Mg/L)
0.000	0.000	7.227	5.524	0.000
0.100	0.100	7.263	5.497	0.000
0.200	0.200	7.296	5.470	0.000
0.300	0.300	7.296	5.443	0.000
0.400	0.400	7.296	5.416	0.000
0.500	0.500	7.296	5.390	0.000
0.600	0.600	7.296	5.363	0.000
0.700	0.700	7.296	5.337	0.000
0.800	0.800	7.296	5.310	0.000
0.900	0.900	7.296	5.284	0.000
1.000	1.000	7.296	5.258	0.000
1.100	1.100	7.296	5.232	0.000
1.200	1.200	7.296	5.207	0.000
1.300	1.300	7.296	5.181	0.000
1.400	1.400	7.296	5.155	0.000
1.500	1.500	7.296	5.130	0.000
1.600	1.600	7.296	5.105	0.000
1.700	1.700	7.296	5.080	0.000
1.800	1.800	7.296	5.055	0.000
1.900	1.900	7.296	5.030	0.000
2.000	2.000	7.296	5.005	0.000
2.100	2.100	7.296	5.000	0.000

FOR THE DISCHARGE AT THE END OF SEGMENT 1
DISCHARGER = South Wales STP (Proposed Facility)
FLOW = .8568 MGD cBOD5 = 3 Mg/L TKN = 3 Mg/L D.O. = 7.6 Mg/L

FLOW FROM INCREMENTAL DRAINAGE AREA = 0.0768 MGD

TOTAL STREAMFLOW = 2.6036 MGD (Including Discharge, Tributaries and Incremental D.A. Flow)

DISTANCE FROM HEAD OF SEGMENT (MI.)	TOTAL DISTANCE FROM MODEL BEGINNING (MI.)	DISSOLVED (Mg/L)	cBODu (Mg/L)	nBODu (Mg/L)
0.000	2.100	7.396	5.823	0.000
0.100	2.200	7.302	5.792	0.000
0.200	2.300	7.302	5.761	0.000
0.300	2.400	7.302	5.730	0.000
0.400	2.500	7.302	5.700	0.000
0.500	2.600	7.302	5.669	0.000
0.600	2.700	7.302	5.639	0.000
0.700	2.800	7.302	5.609	0.000
0.800	2.900	7.302	5.579	0.000
0.900	3.000	7.302	5.549	0.000
1.000	3.100	7.302	5.520	0.000
1.100	3.200	7.302	5.490	0.000
1.200	3.300	7.302	5.461	0.000
1.300	3.400	7.302	5.432	0.000
1.400	3.500	7.302	5.403	0.000
1.500	3.600	7.302	5.374	0.000
1.600	3.700	7.302	5.345	0.000
1.700	3.800	7.302	5.317	0.000
1.800	3.900	7.302	5.289	0.000
1.900	4.000	7.302	5.260	0.000

FOR THE DISCHARGE AT THE END OF SEGMENT 2 DISCHARGER = Fauquier Springs Country Club STP FLOW = .02 MGD cBOD5 = 30 Mg/L TKN = 30.8 Mg/L D.O. = 6 Mg/L

FLOW FROM INCREMENTAL DRAINAGE AREA = 0.0121 MGD

******** RESPONSE FOR SEGMENT 3 ***************

TOTAL STREAMFLOW = 2.6357 MGD (Including Discharge, Tributaries and Incremental D.A. Flow)

DISTANCE FROM HEAD OF SEGMENT (MI.)	TOTAL DISTANCE FROM MODEL BEGINNING (MI.)	DISSOLVED OXYGEN (Mg/L)	cBODu (Mg/L)	nBODu (Mg/L)
0.000	4.000	7.292	5.788	0.913
0.100	4.100	7.279	5.744	0.911
0.200	4.200	7.266	5.700	0.908
0.300	4.300	7.255	5.656	0.906
0.400	4.400	7.244	5.613	0.903
0.500	4.500	7.234	5.570	0.901
0.600	4.600	7.225	5.527	0.898
0.700	4.700	7.216	5.484	0.896
0.800	4.800	7.208	5.442	0.893
0.900	4.900	7.201	5.401	0.891
1.000	5.000	7.194	5.359	0.888
1.100	5.100	7.188	5.318	0.886
1.200	5.200	7.183	5.277	0.883
1.300	5.300	7.178	5.237	0.881
1.400	5.400	7.173	5.196	0.878
1.500	5.500	7.169	5.157	0.876
1.600	5.600	7.166	5.117	0.874
1.700	5.700	7.163	5.078	0.871
1.800	5.800	7.160	5.039	0.869
1.900	5.900	7.158	5.000	0.867
2.000	6.000	7.193	5.000	0.864
2.100	6.100	7.228	5.000	0.862
2.200	6.200	7.261	5.000	0.859
2.300	6.300	7.292	5.000	0.857
2.400	6.400	7.307	5.000	0.854
2.500	6.500	7.307	5.000	0.852
2.600	6.600	7.307	5.000	0.850
2.700	6.700	7.307	5.000	0.847
2.800	6.800	7.307	5.000	0.845
2.900	6.900	7.307	5.000	0.843
3.000	7.000	7.307	5.000	0.840

REGIONAL MODELING SYSTEM 07-20-1998 08:59:59

Ver 3.2 (OWRM - 9/90)

DATA FILE = FAQSP1.MOD

VERSION 3.2

REGIONAL MODELING SYSTEM

DATA FILE SUMMARY

THE NAME OF THE DATA FILE IS: FAQSP1.MOD

Rappahannock River THE STREAM NAME IS: THE RIVER BASIN IS: Rappahannock River

THE SECTION NUMBER IS: 3 THE CLASSIFICATION IS: III

STANDARDS VIOLATED (Y/N) STANDARDS APPROPRIATE (Y/N) = Y

DISCHARGE WITHIN 3 MILES (Y/N) = N

THE DISCHARGE BEING MODELED IS: River Ridge Utility Company STP

PROPOSED LIMITS ARE:

FLOW = .05 MGDBOD5 = 9 MG/L

TKN = 3 MG/LD.O. = 5 MG/L

THE NUMBER OF SEGMENTS TO BE MODELED = 3

7Q10 WILL BE CALCULATED BY: DRAINAGE AREA COMPARISON

THE GAUGE NAME IS: Rappahannock River near Warrenton

GAUGE DRAINAGE AREA

= 195 SO.MI.

GAUGE 7010

= 1.62 MGD

DRAINAGE AREA AT DISCHARGE = 195 SQ.MI.

STREAM A DRY DITCH AT DISCHARGE (Y/N) = N

ANTIDEGRADATION APPLIES (Y/N) = Y

ALLOCATION DESIGN TEMPERATURE = 26 ½C

SEGMENT INFORMATION

SEGMENT # 1

SEGMENT ENDS BECAUSE: A DISCHARGE ENTERS AT END

SEGMENT LENGTH = 2.1 MI

SEGMENT WIDTH = 8 FT SEGMENT DEPTH = 1 FT

SEGMENT VELOCITY = .3 FT/SEC

DRAINAGE AREA AT SEGMENT START = 195 SQ.MI.
DRAINAGE AREA AT SEGMENT END = 204.24 SO.MI.

ELEVATION AT UPSTREAM END = 350 FT ELEVATION AT DOWNSTREAM END = 320 FT

THE CROSS SECTION IS: RECTANGULAR THE CHANNEL IS: MOSTLY STRAIGHT

POOLS AND RIFFLES (Y/N) = N

THE BOTTOM TYPE = SAND SLUDGE DEPOSITS = NONE AQUATIC PLANTS = NONE ALGAE OBSERVED = NONE WATER COLORED GREEN (Y/N) = N

THE DISCHARGE AT THE SEGMENT END IS: South Wales STP (Proposed Facility)

ITS CONCENTRATIONS ARE:

FLOW = .8568 MGD

BOD5 = 3 MG/L

TKN = 3 MG/L

D.O. = 7.6 MG/L

SEGMENT INFORMATION

SEGMENT # 2

SEGMENT ENDS BECAUSE: A DISCHARGE ENTERS AT END

SEGMENT LENGTH = 1.9 MI

SEGMENT WIDTH = 13 FT SEGMENT DEPTH = 1 FT

SEGMENT VELOCITY = .3 FT/SEC

DRAINAGE AREA AT SEGMENT START = 204.24 SQ.MI.
DRAINAGE AREA AT SEGMENT END = 205.7 SQ.MI.

ELEVATION AT UPSTREAM END = 320 FT ELEVATION AT DOWNSTREAM END = 300 FT

THE CROSS SECTION IS: RECTANGULAR THE CHANNEL IS: MOSTLY STRAIGHT

POOLS AND RIFFLES (Y/N) = N

THE BOTTOM TYPE = SAND

SLUDGE DEPOSITS = NONE

AQUATIC PLANTS = NONE

ALGAE OBSERVED = NONE

WATER COLORED GREEN (Y/N) = N

THE DISCHARGE AT THE SEGMENT END IS: Fauguier Springs Country Club STP

ITS CONCENTRATIONS ARE:

FLOW = .02 MGD

BOD5 = 30 MG/L

TKN = 30.8 MG/L

D.O. = 6 MG/L

SEGMENT INFORMATION

SEGMENT # 3

SEGMENT ENDS BECAUSE: THE MODEL ENDS

SEGMENT LENGTH = 3 MI

SEGMENT WIDTH = 18 FT SEGMENT DEPTH = .8 FT

SEGMENT VELOCITY = .3 FT/SEC

DRAINAGE AREA AT SEGMENT START = 205.7 SQ.MI.
DRAINAGE AREA AT SEGMENT END = 208 SO.MI.

ELEVATION AT UPSTREAM END = 300 FT ELEVATION AT DOWNSTREAM END = 285 FT

THE CROSS SECTION IS: RECTANGULAR THE CHANNEL IS: MOSTLY STRAIGHT

POOLS AND RIFFLES (Y/N) = N

THE BOTTOM TYPE = SAND
SLUDGE DEPOSITS = NONE
AQUATIC PLANTS = NONE
ALGAE OBSERVED = NONE

WATER COLORED GREEN (Y/N) = N

REGIONAL MODELING SYSTEM 07-20-1998 09:01:22

Ver 3.2 (OWRM - 9/90)

P. O. Box 11143

SUBJECT: Stream Analysis - Fauquier Springs Country Club

TO:

Ernie Watkins - NRO

FROM:

Martin G. Ferguson Jr.

DATE:

February 10, 1988

COPIES:

Burt Tuxford, Steve Crowther - NRO

We have reviewed the stream analysis for the Fauquier Springs Country Club discharge to the Rappahannock River submitted on January 26, 1988.

The model is approved for use and we have no problem with the permit limits determined.

brt24/sph



BY NCRTHERN REGIONAL OFFICE

RANUUM

State Water Control Board

2111 North Hamilton Street

P. O. Box 11143

Richmond, VA. 23230

SUBJECT: Stream Analysis for Fauquier Springs Country Club

TO:

Martin Ferguson, Jr. - OWRM

FROM:

Steve Crowther - NROC

DATE:

January 26, 1988

Please find attached a stream analysis for OWRM review and comment.

Attachment

2111 North Hamilton Street

State Water Control Board

P. O. Box 11143

Richmond, VA. 23230

SUBJECT: Stream Analysis for Fauquier Springs Country Club

TO:

Dale Phillips, OWRM

FROM:

Steve Crowther, NROC

DATE:

January 26, 1988

An NPDES permit application has been received for discharge of effluent from the Fauquier Springs Country Club lagoon directly to the Rappahannock River. The lagoon design flow is 17,430 GPD based on a 25 day detention time. This facility has been in existence for more than twenty years.

The Q7-10 for the Rappahannock River at the discharge point is approximately 1.58 MGD, the slope is 5 ft/mile, and the elevation is 300 feet. A velocity of 0.25 ft/sec has been assumed. background BOD, data for the Rappahannock River was obtained from the Remington (12-10-87) model.

Attached are four model simulations. The STP discharge data was first assumed as $BOD_s = 30 \text{ mg/l}$, TKN = 18 mg/l, and DO = 6.5 mg/l. K2 is 3.0 day and K1 and Kn are 0.11 day. The first simulation was run with good results. In the second simulation, In the third, the K2 value was the DO was dropped to 6.0 mg/l. halved, K1 and Kn doubled, with DO = 6.0. In the fourth run, the TKN discharge value was increased to 24 mg/l with K2 halved, K1 and Kn doubled, and DO = 6.0 mg/l. All of the simulations gave good results with a maximum deficit \approx .17 mg/l.

Because the lagoon has a 25 day detention time, I expect that warm weather TKN effluent values will be low even though I incorporated a TKN value of 21 mg/l into the model. Since the model results will protect the river from degradation, it appears TKN does not need to be a permit parameter at this time.

 $BOD_5 = 30 mg/1$ $TSS^5 = 30 mg/1$ Therefore, the proposed permit limits are:

= 6.0 mg/lDO

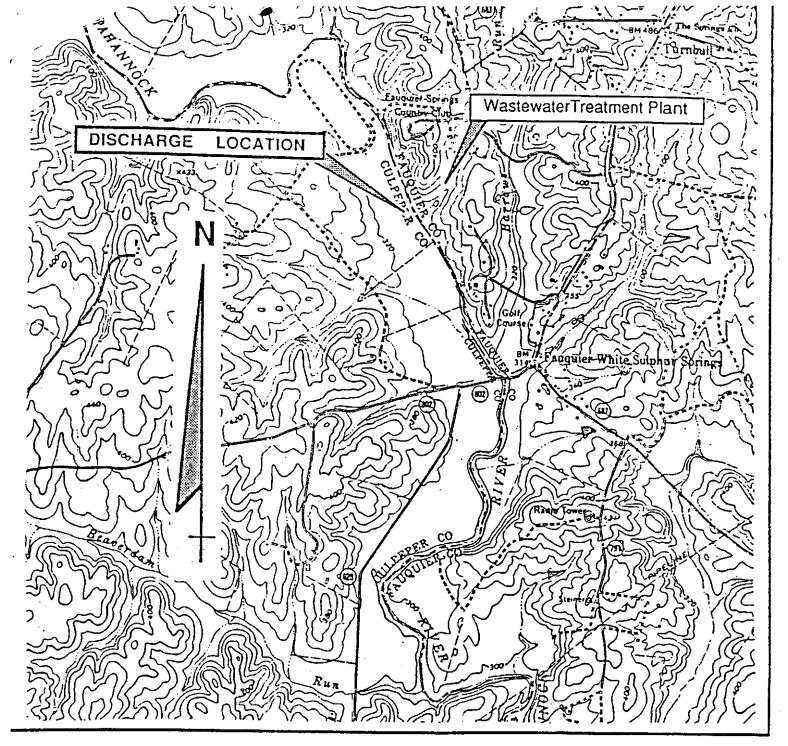
Attachment

Kennington STP Model

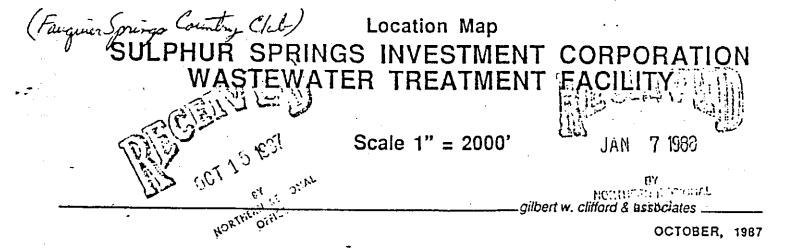
BACKGROUND STREAM DATA FOR BOD RAPPAHANNOCK RIVER AT REMINGTON

DATE	В	DO	(mg/l)
1/84			2
2/84			2
3/84			1
4/84			2
5/84	*	•	2
7/84			ī
8/84			3
9/84			1
10/84	•		1
11/84			1
12/84			3
1/85			1
3/85			1
4/85			1
6/85			1
7/85			1
2/86	•		1
3/86			1
4/86 5/86			1
6/86			1
7/86			2
8/86			1
3,00		,	4
	TOTAL		34

TOTAL 34 AVERAGE 1.5



From U. S. G. S. "Warrenton" and "Jeffersonton" Quadrangles



THE BACKGROUND CONDITIONS ARE: ______

A THE SECOND OF THE SECOND OF

FLOW: 1.5800 MGD 0.0.0 6.875 MG/L CBODA: 3.75 MG/L MBODus 0.87 MG/L

OUTPUT VILL BE GENERATED EVERY 0.20 MILE FROM THE BEGINNING OF A SEGNENT

THE VARIABLES FOR SECTION 1 APE: ************

SECHENT LENGTH . 3.00 HI YELOCITY . 4.091 HI/D TEMP. = 30.0 °C ELEV = 300.00 FT SATURATION D.O. = 7.639 HG/L Ea = 3.000 /DAY Er = 0.110 /DAY En = 0.110 /DAY

The k rates shown are at 20 degrees C. The model corrects thes.

FOR THE DISCHARGE AT THE BEGINNING OF THE SECREPTS

FLOR= 0.0174 MGD D.O.= 6.50 MG/L CBODu= 75.00 MG/L MBODu= 65.00 MG/L

DISTANCE (MI) FROM MEAD OF SEGMENT	DATOT DISTANCE (HI) FROM DESINATION DESINATION	D.O. (mg/l)	CBODe (ng/1)	HB00w (mg/1)
0.000	0.000	(6.87)	4.527	1.570
0.200	0.200	6.950	4.469	1.552
0.400	0.400	7.016	4,451	1.534
0.600	0.600	7.071	4.413	1.536
0.000	0.800	7.117	4.376	1.499
1.000	1.000	7.156	4.339	1.481
1.200	1,200	7.189	4.302	1.464
1.400	1.400	7.216	4.266	1.447
1,600	903.1	7.240	4.229	1.431
1.800	1.800	7.260	4.194	1.414
2.000	2,000	7.277	4.158	1.396
2.200	1.200	7.291	4.123	1.382
2.400	2.400	7.304	4.084	1.364
2.600	1.600	7.315	4.053	1.350
2.806	2.800	7.324	4.019	1.334
3.000	3.000	7.332	3.965	1.319

STP: c 800 : 30 TKN: 18-3.15 DO = 6.5

Reach = 3.0 mile, relienty = . 25 ft/sec, elevation 300 ft, slope = 5 ft/mi. X2 : (.025)(24)(5 ft/mi) = 3 day "

MODEL SINULATION FOR THE FAUGULER SPRINGS COUNTRY CLUB DISCHARGE TO

THE BACKGROUND CONDITIONS ARE: ------

FLOW: 1.5800 BGD B.O.= 6.875 BG/L CBODU= 3.75 BG/L BBODU= 0.87 BG/L

OUTPUT WILL BE GENERATED EVERY 0.20 MILE FROM THE REGINNING OF A SEGNENT

THE VARIABLES FOR SECTION 1 ARE: ------

SECHENT LENGTH . 3.00 MI VELOCITY . 4.091 MI/D TEMP. = 30.0 °C ELEY = 300.00 FT SATURATION D.O. = 7.639 MG/L Es = 3.000 /DAY Er = 0.110 /DAY En = 0.110 /DAY

0	************	LEGE AT THE BEG		GRENT: 75.00 BG/L MBG/	N= 65.00
2)	THE RI	SULTS FOR SECTION			• • • • •
*3	DISTANCE (HI) FROM HEAD OF SEGMENT	TOTAL DISTANCE (HI) FROM BEGIRBING	0.0. (mg/l)	CBODu (ag/l)	HBC (ag/
	0.000	0.000	6.865	4,527	1.5
	0.200	0.200	£.945	4,459	1.5
j (3)	0.400	0.400	7.012	4.451	1.5
ز: ا	0.600	0.600	7.068	4.413	1.5
1	0.800	0.800	7.314	4.376	1.4
j W	1.000	1.000	7.154	4.339	1.4
39	1.200	1.200	7,187	4.302	1.40
	1.400	1.400	7.215	4.266	1.4
O	1,600	1.600	7.239	4.229	1.43
೦	1.800	1.600	7.259	4.194	1.41
G	2.000	. 2.000	7.276	4.158	1.39
	2.200	2.200	7.291	4.123	1.38
O	2.100	2,400	7.303	4.088	1.36
0	2.600	2.600	7.314	4.053	1.35
9	2.800	1.800	7.324	4.015	1.33
છ	1.000	3,000 13,000	7.332	3.985	1.31

In this simulation the STP DO have been reduced to 6.0 mg/h.

1	40	HOLTAJUHIZ	COMPLETED				
		MODEL SIMULATION FOR THE FAUGUIER SPRINGS COUNTRY CLUB DISCHARGE TO RAPPARAMHOCK RIVER					
	ツラ (人)	THE BACKGROUND CONDITIONS ARE.					
ik:	ું 🤊	FLOW- 1.5000 MCD B.O. = 6.875 MG/L CBODu- 3.75 MG/L MBODe- 0.87 MG/L					
	9 9	OUTPUT WILL BE GENERATED EVERY O. 20 MILE FROM THE BECLIBERED OF A COMME					
		THE VARIABLES FOR SECTION 1 ARE:					
		SEGMENT LENGTH : 3.00 MI VELOCITY : 4.091 MI/D TEMP 30.0 - C FIFY : 300 MI T SERVINGEROUS					
	3 3	The k rates shown are at 20 degrees C. The sodel corrects thea.					
	3	•	HARGE AT THE B	ECITATING OF THE	SEGNENT:		
27						RB0Du= 65.00 HG/L	
	() ()	: • • • • • • • • • • • • • • • • • • •	• • • • • • •	• • • • • • • • •		• • • • • • • •	
	9	*****	SULTS FOR SECT	FION 1 ARE:			
		DISTANCE (RI) FROM	TOTAL DISTANCE				
	25	BEAD OF SECHENT	INI) FROM BECIENTEG	D.O. (ag/l)	CB0Du (mg/1)	NB00u	
	9		********	*****	189713	(mg/1)	
S i) 1	0.000	0.000	6.865	4.527	1.570	
ġ.	1 10	0.200	0.200	6.827	4.451	1.534	
	ا وتاي	0.400	0.400	6.794	4.376	1.499	
		0.600	0.600	6.765	4.302	1.464	
	(u)	0.800	0.800	6.741	1.229	1.411	
	3	1.000	1.000	6.722	4.158	1.398	
(7.7.	•	1.200	1.200	6.705	4.088	1.366	
	•	1.400	1.400	6.692	4.019	1.334	
	9	1.600	1.600	6.642	3.951	1.304	
j. 60	_	1.800	1.800	6.675	3.884	1.274	
	0	2.000	2.000	6.679	3.819	1.244	
	0	2.200	2.200	6.667	3.754	T.216	
		2.400	2.400	ONS (NO.)	3.691	1.164	
網	0	2.500	2.600	1.667	3.629	1.161	
Ť.	O	2.600	2.600	6.679	3.567	1.134	
ξ, / J		1 000					

c BOD : 30 TKN : 18-3:15 DO : 6

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73	RECOLL STRUCTURES FOR THE PAUDULE SPRINGS COUNTRY CLUB DISCHARGE TO STRUCTURE STRUCTUR						
D	THE BICKS	room combilions	182:				
1		5800 MGB D.O. = 6					
うっ	THE PARTAS	LL BE GENERATED E	1 ARE:	FROM THE BEGINNI	NG OF A SEGNERY		
9	SEGMENT LENGTH = 3.00 MI VELOCITY = 4.091 MI/D TEMP. = 30.0 °C ELEY = 300.00 FT SATURATION D.O. = 7.639 MG/L La = 1.500 /DAY Er = 0.220 /DAY En = 0.220 /DAY						
0	The k cate	s shown are at 20 SCHARGE AT THE BI	degrees C. The	model corrects	thes.		
10	******	174 MGD D.O. • (.00 MG/IL CBODU		ODu= 91.00 HG/L		
3		RESULTS FOR SECT	ION 1 ARE:				
	DISTANCE	TOTAL.					
÷5	HEAD OF				•		
	SEGNENT	BEGINNING (KI) FROM	D.O. (mg/l)	CBOD _M	KBOD*		
1100				(ag/L)	(ag/1)		
٠. ن	0.000	0.000	6.865	4.527	1.853		
	0.200	0.200	6.821	4.451	1.811		
*	0.400	0.400	6.782	4.376	1.769		
્છ	0.600	0.600	6.749	4.302	1.729		
	0.800	0.600	6.720	4.229	1.689		
49	1.000	1.000	6.697	4.158	1.650		
⇔	1.200	1.200	6.677	4.088	1.612		
	1.400	1.400	6.661	4.019	1.575		
Ð	1.600	1.600	6.649	3.951	1.539		
6	1.800	1.800	6.639	3.864	1.504		
	2.000	2.000	6.432	3.819	1.469		
Ð	2.200	2.200	6.628	3.754	1.436		
0	2.400	2.400	(5.126 p.G	3.691	1.403		
	2.600	2.600	(1.11)	3.629	1.370		
3	2.800	2.800	6.627	3.567	1.309		
N	1.000	1.000	6-630	3.507	1 300		

CBOD = 30 TKN > 24-3=21-7R Da = 6.0

In the simulation, the NBOB. her been increased from 65-1/2 to 91.00 mg/L. The result appeared to be relatively increasitive to the change.

Conclusion: The proposed permet limit au:

cBODs = 30

TKN = No permet limit necessary

DO = 6.0 mg/L

Public Notice - Environmental Permit

PURPOSE OF NOTICE: To seek public comment on a draft permit from the Department of Environmental Quality that will allow the release of treated wastewater into a water body in Fauquier County, Virginia.

PUBLIC COMMENT PERIOD: XXX, 2014 to XXX, 2014

PERMIT NAME: Virginia Pollutant Discharge Elimination System Permit – Wastewater issued by DEQ, under the authority of the State Water Control Board

APPLICANT NAME, ADDRESS AND PERMIT NUMBER: Sulphur Springs Investment Corporation, P. O. Box 419, Warrenton, VA 20186, VA0077411

PROJECT DESCRIPTION: Sulphur Springs Investment Corporation has applied for a reissuance of a permit for the private Fauquier Springs Country Club WWTP. The applicant proposes to release treated sewage wastewaters from private country club and golf course at a rate up to 0.02 million gallons per day into a water body. The sludge will be disposed by transporting it to Fauquier County Water and Sanitation Authority's Remington Regional Wastewater Treatment Plant (VA0076805) for processing and disposal. The facility proposes to release treated sewage in the Rappahannock River in Fauquier County in the Rappahannock River watershed. A watershed is the land area drained by a river and its incoming streams. The permit will limit the following pollutants to amounts that protect water quality: pH, BOD₅, Total Suspended Solids, Dissolved Oxygen, Ammonia as N, and E. coli bacteria.

HOW TO COMMENT AND/OR REQUEST A PUBLIC HEARING: DEQ accepts comments and requests for public hearing by hand-delivery, e-mail, fax or postal mail. All comments and requests must be in writing and be received by DEQ during the comment period. Submittals must include the names, mailing addresses and telephone numbers of the commenter/requester and of all persons represented by the commenter/requester. A request for public hearing must also include: 1) The reason why a public hearing is requested. 2) A brief, informal statement regarding the nature and extent of the interest of the requester or of those represented by the requester, including how and to what extent such interest would be directly and adversely affected by the permit. 3) Specific references, where possible, to terms and conditions of the permit with suggested revisions. A public hearing may be held, including another comment period, if public response is significant, based on individual requests for a public hearing, and there are substantial, disputed issues relevant to the permit.

CONTACT FOR PUBLIC COMMENTS, DOCUMENT REQUESTS AND ADDITIONAL INFORMATION: The public may review the draft permit and application at the DEQ-Northern Regional Office by appointment, or may request electronic copies of the draft permit and fact sheet.

Name: Joan C. Crowther

Address: DEQ-Northern Regional Office, 13901 Crown Court, Woodbridge, VA 22193 Phone: (703) 583-3925 E-mail: joan.crowther@deq.virginia.gov Fax: (703) 583-3821